THE EVALUATION OF THE EFFECTS OF SEISMIC DETONATIONS ON WATER WELLS

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Edmonton, Alberta

April, 1979

CONTENTS

	Page
Background and history	1
Scope and objectives	2
Exploration and final site selection	3
Project site description	5
Drilling and well details	5
General geology	9
General hydrogeology	9
Testing methods and sequences	11
Pre-detonation hydrogeological characteristics	13
Aquifer characteristics	13
Well characteristics	23
Groundwater quality	24
Water level fluctuations	37
Post-detonation hydrogeological characteristics	37
Aquifer characteristics	37 [.]
Well characteristics	38
Groundwater quality	39
Water level fluctuations	40
Conclusions	44
Well and aquifer characteristics	45
Well yield and depth	45
Water quality	45
Water level fluctuations	46
Recommendations	46
Acknowledgements	47
References	47
Appendix A. Original project proposal, and exploration and project site drilling	
Appendix B. Pre-detonation aquifer and well performance tests	
Appendix C. Post-detonation aquifer and well performance tests	
Appendix D. Hydrochemical data - summaries and analyses	

ILLUSTRATIONS

			Page
Figure	1.	Location map	4
Figure	2.	Well layout	6
Figure	3.	Geological cross section	7
Figure	4.	Lithological and electrical well logs	8
Figure	5.	Water level fluctuations	
Figure	6a.	Composite drawdown plots for DSAT pumping well	14
		Composite drawdown plots for DSAT observation well	
		Composite drawdown plots for DSAT pumping well	16
		Composite drawdown plots for DSAT observation well	17
	6e.	Composite drawdown plots for BOHAT pumping well	18
		Composite drawdown plots for BOHAT observation well	19
		Composite drawdown plots for BOHAT pumping well	20
		Composite drawdown plots for BOHAT observation well	21
Figure		Analysis of well performance test DSWT 1	26
		Analysis of well performance test DSWT 5	27
		Analysis of well performance test BOHWT 1	28
		Analysis of well performance test BOHWT 5	29
		Analysis of well performance test BSCWT 1	30
	7f.	Analysis of well performance test BSCWT 5	31
Figure		Chemical variations during DSAT	32
		Chemical variations during BOHAT	33
	8c.	Chemical variations during DSWT	34
	8d.	Chemical variations during BOHWT	35
	8e.	Chemical variations during BSCWT	36
Figure	9.	Water level fluctuations during detonations	41
		Post-testing water level fluctuations	43
		*	
		TABLES	
Table 1	. 4	Well Testing Sequence	12
Table 2		Results of Drift Aquifer Performance Tests	13
Table 3		Results of Bedrock Aquifer Performance Tests	22
Table 4		Results of Well Performance Tests	25

BACKGROUND AND HISTORY

In the last twenty-five years, the Government of Alberta and more specifically, the Geophysical Inspections Branch of Energy and Natural Resources (formerly Department of Mines and Minerals), have been receiving complaints concerning alledged damage to domestic water wells by seismic detonations associated with petroleum exploration. The number of these complaints has generally increased and in the past few years the Geophysical Inspections Branch has literally been inundated with damage claims. For example, in 1977 and 1978, respectively, a total of 144 and 220 claims concerned with water well damage were received and processed.

For the past ten years the Groundwater Division of the Alberta Research Council has acted as an impromptu advisor and consultant to the Geophysical Inspections Branch concerning these well damage claims. This liaison has included site inspections, aquifer and well testing, teaching basic methods of hydrogeological evaluation and outlining procedures for scientifically evaluating the claims. As a result of this consultation, a logical and scientific procedure to investigate these claims, presented in February 1978 by G. M. Gabert (pers. comm.), will be issued as a procedural directive by Energy and Natural Resources (E&NR).

Unfortunately, in spite of a good general knowledge of domestic water wells and aquifers in Alberta, most of the claims have to be processed with little or no specific information concerning the original hydraulic parameters, construction and efficiency of a particular well. In light of this, settling such claims can be a frustrating and formidable task. In the summer and fall of 1978, therefore, a number of projects concerned with determining the effects, if any, of seismic activity on water wells were initiated by E&NR. This report describes the project completed by the Alberta Research Council, Groundwater Division, near New Norway, Alberta in October, November and December, 1978.

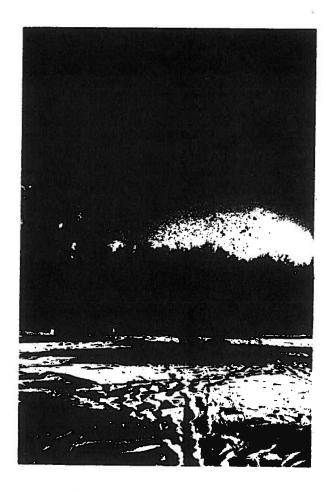
SCOPE AND OBJECTIVES

The scope and objectives for the New Norway seismic project were formulated in various correspondence between Energy and Natural Resources and the Groundwater Division, Alberta Research Council but are probably best outlined in a memorandum by Gordon Gabert dated May 17, 1978 (App. A).

The main objective of the project was to attempt to scientifically evaluate the effects of seismic detonations on water wells and thus aid E&NR in evaluating claims of well damage. According to complaints received, the most common parameters affected were water levels, groundwater chemistry, well hydraulics, well depths, groundwater appearance or smell and well yield. A secondary objective of the project was to establish how far from water wells seismic detonations should take place in order to minimize or eliminate possible damaging effects. This objective would therefore attempt to verify the present legal distance of 183 m.

In establishing the scope of the project, it was important to operate under conditions that were as typical of Alberta as possible. The project was to be located in a plains environment typical of Alberta. A line of four wells were to be completed; two in a typical bedrock aquifer such as a bentonitic sandstone, and two in a typical drift aquifer such as sand or sand and gravel. Well construction was to be either slotted casing or open hole as is common in most domestic water wells in Alberta. Three or four shotholes, 18 m deep, were to be drilled in a line at right angles to the line of water wells and loaded with 4.5 kg of explosive. Well and aquifer conditions were to be evaluated by aquifer and well performance tests prior to detonation. After each detonation, well conditions were to be re-evaluated using the same sequence of aquifer and well performance tests. A down-the-hole camera, supplied by Alberta Environment, would be used to inspect wells after every detonation.

NEW NORWAY SEISMIC PROJECT



The 4.6 m shothole detonation. Continuous water level recorder shown in background. This photo was taken a few seconds after the cover photo.

EXPLORATION AND FINAL SITE SELECTION

After receiving bids from five water well drilling contractors, Schmidt Drilling Ltd. of Tees, Alberta was selected to complete the drilling portion of the project.

As mentioned previously, one of the basic requirements of the project site was that it be typical of Alberta conditions and be underlain by bedrock and drift aquifers suitable for hydrogeological testing. This requirement of two typical aquifers at one site proved rather stringent and the first two weeks of the field portion of the project consisted of exploring for a suitable location. The search area had been narrowed somewhat in that the suitable bedrock was thought to be Horseshoe Canyon Formation at a location within 160 km of Edmonton. The requirement that a drift aquifer of sufficient size be present generally indicated that a buried valley of some description should also be present at the site. On this basis, an area southwest of Camrose, which was underlain by Horseshoe Canyon Formation and traversed by the Red Deer buried valley, was selected for exploration. Pertinent details of the exploration sites are in appendix A.

The first site, located at NW-17-44-21 W4M (Fig. 1), or about 12 km southwest of New Norway, was drilled on October 17, 1978. Wells in bedrock and drift were completed the same day. Drift consists of 15 m of till and clay which yielded approximately 10 cubic meters per day (m³/d) during airlifting. Bedrock consists of a sandstone and shale sequence which yielded 80 to 130 m³/day during airlifting. Because of the lack of a suitable drift aquifer the site was abandoned.

The second and third sites (Fig. 1) were located about 6 km southeast of New Norway at NW-25-44-21 W4M and SE-25-44-21 W4M. The second site was located in the northern portion of a meltwater channel in order to locate a suitable drift aquifer. The drift, however, consists of 11 m of till and clay which yielded no groundwater. Bedrock, on the other hand, consists of sandstone and shale, and yielded approximately 70 m³/day. This site was also abandoned.

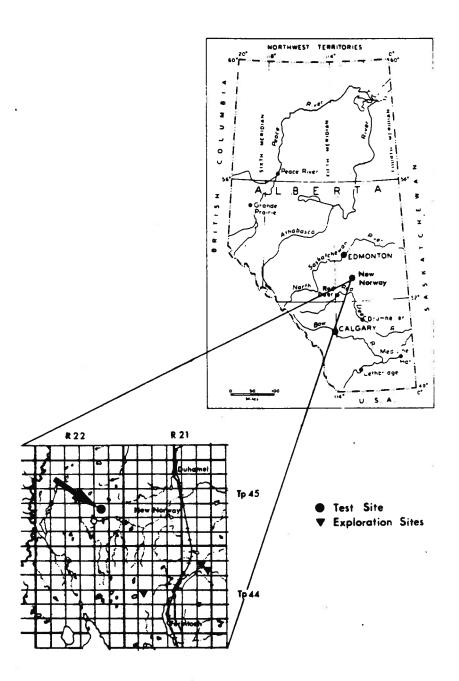


Fig. 1 Location map

The third site was located on the south side of the same meltwater channel. Here, three wells were drilled to depths of 39, 43 and 79 m. The drift, approximately 40 m thick, consists of till, clay, sand and gravel and contained two excellent gravel aquifers between 30 m and 40 m below surface. Using a completion of slotted casing, the top gravel aquifer yielded 200 m³/day during airlifting. After completion of the drift wells, a bedrock well was drilled to a depth of 79 m in a sequence of shale and sandstone which only yielded 10 m³/day during airlifting. Because of this, the site was abandoned.

The final exploration site, which ultimately became the project site (Fig. 1) was located 10 km west of New Norway at 11-14-45-22 W4M. A total of four wells were drilled; two to 25 m and two to 73 m. Approximately 25 m of drift is present and consists of till, clay, and a basal, 3.3 m thick, sand and gravel aquifer. During airlifting the gravel aquifer produced approximately 45 m³/day. Bedrock encountered during drilling consisted of sandstone, siltstone, shale and coal seams which produced approximately 15 m³/day during airlifting. Although the yield of the bedrock was low, it was considered to be adequate and this location was therefore selected as the project site.

PROJECT SITE DESCRIPTION

Drilling and Well Details

Exploration drilling of the project site commenced on October 30, 1978. The initial pilot holes which were sampled every 1.5 m and electrically logged, were reamed, cased and airlifted to complete the project wells. The resulting four wells were located in a north-south line 15 m apart (Fig. 2). The drift wells were the northern two wells and were identified as DS (drift south) and DN (drift north). Well completion in both cases consisted of 140 mm diameter casing slotted between 22 m and 25 m below ground surface (Figs. 3 & 4). The driller was instructed to cut a typical slot pattern in this 3 m interval, but on inspection the number of slots was increased. In this regard the completion of the drift wells was not, strictly speaking, typical. The bedrock wells were the southern pair and were identified as BOH (bedrock open hole) and

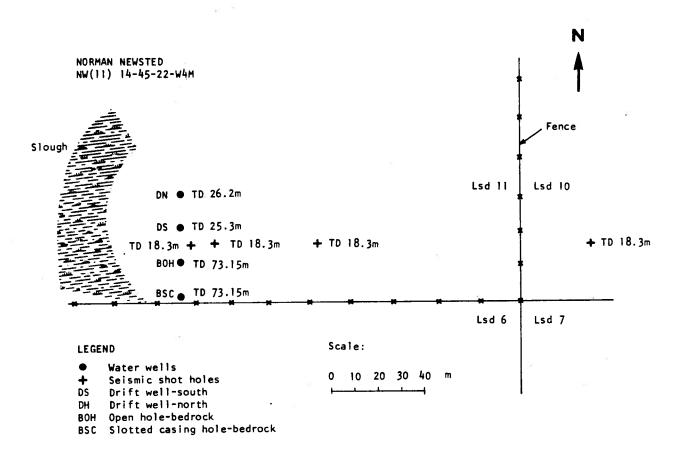


Fig. 2 Well layout

BSC (bedrock slotted casing). Both bedrock wells were drilled to a depth of 73 m (Figs. 3 & 4). Well BOH was completed using 140 mm diameter casing to a depth of 27 m and open hole completion to the bottom of the well. Well BSC was completed using 140 mm diameter casing from surface to 30 m and a 114 mm diameter slotted liner from 28 m to the bottom of the well. In the case of BSC the driller was instructed to slot the liner in a typical pattern which was not subsequently modified. In order to be compatable with domestic water wells no cementing was done during well construction, rather casing seals were attempted by driving casing into the appropriate shale beds.

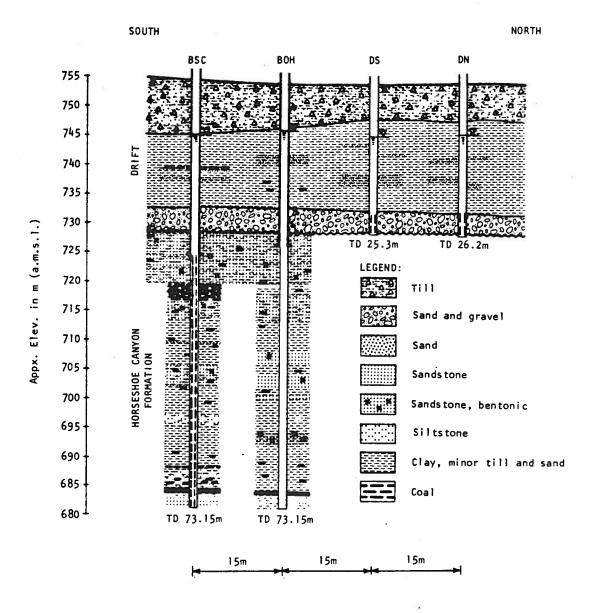


Fig. 3 Geological cross section

Problems occurred during development of the drift aquifer. During airlifting large amounts of sand entered wells DS and DN and between 6 and 8 hours were required to complete development of each well. This is probably atypical when compared to domestic water wells. In spite of development, sand continued to enter well DS during pumping and its total depth was therefore decreasing slightly



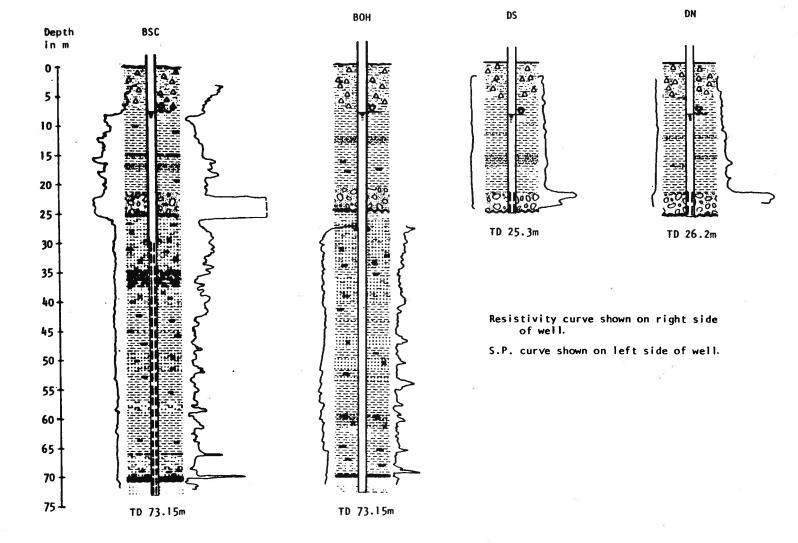


Fig. 4 Lithological and electrical well logs

during testing. Development of the bedrock wells consisted of washing and airlifting each well for approximately two to three hours. Well BOH, probably because of the open hole completion, bridged at 59 m a few days before detonation began.

Shotholes were drilled in an east-west line at distances of 183, 61, 15, and 4.6 m away from the line of wells (Fig. 2). Shotholes were drilled to a depth of 18 m and loaded with 4.5 kg of explosive. The completion of shotholes in the drift was atypical of seismic exploration procedures in Alberta.

General Geology

The project site occurs in an area underlain by the preglacial Red Deer River valley and Cretaceous Horseshoe Canyon Formation bedrock. The site was approximately 3 km north of the center line of this preglacial valley and is shown by Stalker (1960) to be underlain by a total drift thickness of between 23 and 28 m. The succession of drift underlying the site (Figs. 3 & 4) consists of lake clays, tills, intertill sands and gravels, and preglacial sands and gravels. It is assumed that the basal sand and gravel aquifer, tested during the project, is preglacial in spite of granitic fragements being present in drill cuttings. Contamination from overlying intertill sands and gravels, during drilling, is suspected. The sand and gravel aquifer is composed of medium to coarse dark gray sand in a matrix of well rounded pebbles of chert and limestone up to 75 mm in diameter.

The bedrock consists of fine to medium grained bentonitic sandstones, dark colored shales, minor siltstone and the occasional coal seam (Figs. 3 & 4). The down-the-hole camera showed that in the open hole (BOH), sandstone and siltstone layers preferentially cave compared to shales and coals.

General Hydrogeology

The main aquifers tested during the project were the basal sand and gravel in the drift and a collection of small, indistinct aquifers in the bedrock (Figs. 3 & 4). The sand and gravel aquifer is confined, having a potentiometric surface

approximately 8.3 m below ground surface. The bedrock "aquifer" is composed of several thin low yielding zones which include a sandstone at 38 m, a shale at 44 m, a sandstone at 54 m and a coal seam at 70 m. The combined potentiometric surface for these aquifers is 8.6 m below ground surface. Pre-testing water level fluctuations (Fig. 5) indicated that both bedrock and drift aquifers were responsive to changes in barometric pressure.

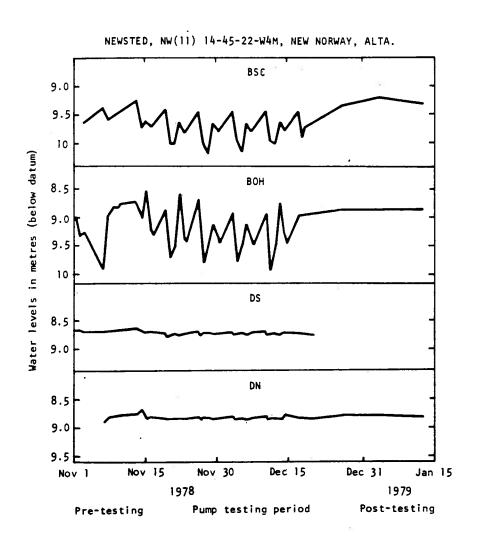


Fig. 5 Water level fluctuations

Assuming wells BOH and DS are at the same elevation a small downward hydraulic gradient exists under the project site. In addition, regional groundwater movement is probably towards the south into the topographic low which coincides with the thickest portion of the preglacial valley.

Both aquifers have total dissolved solids concentrations in the range 1400 to 1700 mg/l. The drift aquifer groundwater is of poor quality because of high concentrations of iron, sulfate, hardness, and alkalinity. Bedrock groundwaters are of slightly better quality but have high concentrations of sodium, sulfate, iron, and alkalinity.

TESTING METHODS AND SEQUENCES

As previously mentioned, the basic purpose of this project was to evaluate the effects (if any) of seismic detonations on water wells. It was felt that any such effects could best be measured by calculating aquifer characteristics and well characteristics prior to any detonations and after each individual detonation.

Aquifer characteristics were calculated by means of constant rate, twelve hour aquifer performance tests conducted in both the drift and bedrock wells. Tests of the bedrock aquifer were completed using well BOH as the pumping location and well BSC as the observation well. Tests of the drift aquifer were completed using well DS as the pumping location and well DN as the observation well. During aquifer performance tests all wells were monitored to evaluate interaction between drift and bedrock aquifers. Recovery measurements were taken after all aquifer performance tests and, in some cases, analyzed (App. B & C).

Well characteristics were calculated by means of variable rate, well performance (step-drawdown) tests consisting of five 100-minute pumping intervals at successively higher pumping rates. For well DS these steps were completed at 10.9, 21.8, 32.7, 43.6, and 54.5 m³/day and for wells BSC and BOH the appropriate pumping rates were 2.725, 5.45, 8.175, 10.9, and 13.625 m³/day. Water levels were measured in all wells during all well performance tests. Time-drawdown plots are shown in appendices B and C.

Aquifer and well performance tests were completed in a set sequence as shown in table 1. These testing sequences were numbered according to whether they were pre-detonation (all tests ending with number one) or post-detonation (all tests ending with numbers two through five). Appropriate examples are BOHAT 1 (bedrock open hole aquifer test 1) or DSWT 4 (drift south well test 4). Table 1 shows the testing sequence adopted, as well as dates and test numbers in relation to the particular shothole detonations.

Table 1. Well Testing Sequence - New Norway Seismic Project

	20					
Pre-detonation Nov 14-20, 1978	BSCWT 1	DSWT 1	BOHWT 1	DSAT	1	BOHAT 1
	183	metre shothole	detonation,	November	21,	1978
Post 183 metre detonation Nov 21-27, 1978	BSCWT 2	DSWT 2	BOHWT 2	DSAT	2	BOHAT 2
	61	metre shothole	detonation,	November	28,	1978
Post 61 metre detonation Nov 28-Dec 4,1978	BSCWT 3	DSWT 3	BOHWT 3	DSAT	3	BOHAT 3
	15	metre shothole	detonation,	December	5,	1978
Post 15 metre detonation Dec 5-11, 1978	BSCWT 4	DSWT 4	вонут 4	DSAT	4	BOHAT 4
	4.6	metre shothole	detonation,	December	12,	1978
Post 4.6 metre detonation Dec 12-18, 1978	BSCWT 5	DSWT 5	вонут 5	DSAT	5	BOHAT 5

BSC = Bedrock slotted casing, BOH = Bedrock openhole,

DS = Drift south, DN = Drift north

WT = Step-drawdown well test, 5 steps, 100 minutes per step

AT = Aquifer test, constant flowrate, 12 hours duration

Groundwater samples were collected thirty minutes after the start of each test and a few minutes before the end of each test. Well depths were measured after each weekly set of tests. Detonation of the appropriate shothole then occurred, well depths were remeasured, and wells were logged with the down-the-hole camera. During shothole detonation, continuous water level recorders were operating in order to measure the effects of detonation on the water levels in the wells.

Aquifer performance tests were analyzed using the type curve method (Theis, 1935) and the modified non-equilibrium method (straight line) of Cooper and Jacob (1950). Well performance tests were analyzed using a type curve method (Sheahan, 1971), a graphical procedure (Bierschenk and Wilson, 1961) and a computer method (Labadie and Helweg, 1975).

PRE-DETONATION HYDROGEOLOGICAL CHARACTERISTICS

Aquifer Characteristics

Pre-detonation aquifer characteristics were evaluated by analyzing drawdown (and occasionally recovery) data from aquifer performance tests DSAT 1 and BOHAT 1 (App. B). Time-drawdown plots of these tests, inter alia, are also shown in figures 6a to 6h.

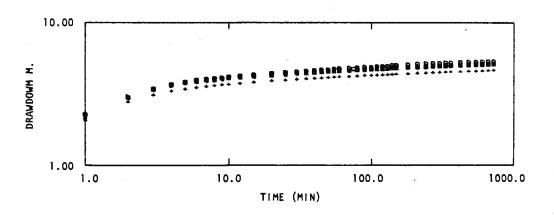
Table 2 shows at the top, drift aquifer parameters obtained from the analysis of DSAT 1. Using the data from the observation well (well DN), the sand and

	Pumpi	ng Wel	l (Well	DS)	Observation Well (Well DN)				
		Straight Line		Type Curve		raight . Line		ype urve	
28	T	S	T	s	Т	S	Т	S	
DSAT 1	21.45		13.99	23	17.35	1.52 x 10 ⁻⁵	17.70	1.28 × 10 ⁻⁵	
DSAT 2	19.18		13.55		15.35	1.75 × 10 ⁻⁵	16.18	1.17 × 10-5	
DSAT 3	16.62		12.76		14.46	2.19 x 10 ⁻⁵	16.06	1.16 x 10-5	
DSAT 4	18.82		13.14		15.11	1.73 × 10 ⁻⁵	16.06	1.16 x 10-5	
DSAT 5	14.05		12.68		13.85	2.75 × 10 ⁻⁵	16.06	1.16 × 10 ⁻⁵	

Table 2. Results of Drift Aquifer Performance Tests - New Norway Seismic Project

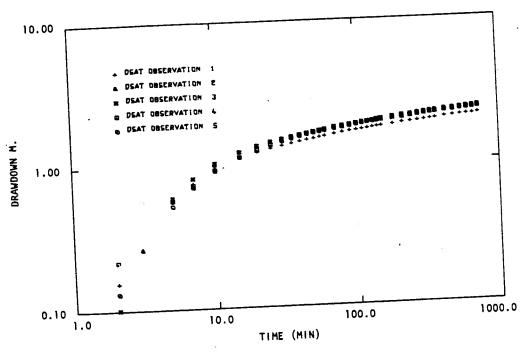
 $T = Transmissivity (m^2/day)$

S = Storativity



					TRANSMISSIVITY (m²/day)
+	DSAT	PUMP	WELL	1	 13.99
•	DSAT	PUMP	WELL	2	 13.55
×	DSAT	PUMP	WELL	3	 12.76
•	DSAT	PUMP	WELL	4	 13.14
•	DSAT	PUMP	WELL	5	 12.68

Fig. 6a Composite drawdown plots for DSAT pumping well



	TRANSMISSIVITY (m2/day)	STORATIVITY
•		1.28 × 10 ⁻⁵
+ DSAT OBSERVATION 1		1.17 × 10 ⁻⁵
a DSAT OBSERVATION 2		1.16 x 10 ⁻⁵
# DSAT OBSERVATION 3	16.00	1.16 x 10 ⁻⁵
DSAT OBSERVATION 4	. 16.00	1.16 × 10 ⁻⁵
DSAT OBSERVATION 5	. 16.06	1110

Fig. 6b Composite drawdown plots for DSAT observation well

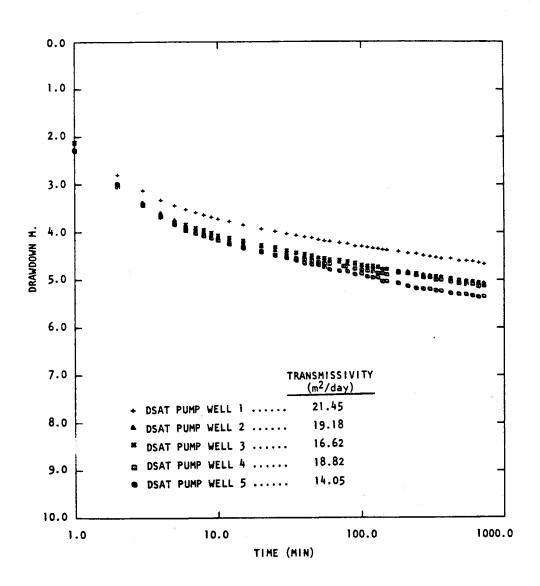


Fig. 6c Composite drawdown plots for DSAT pumping well

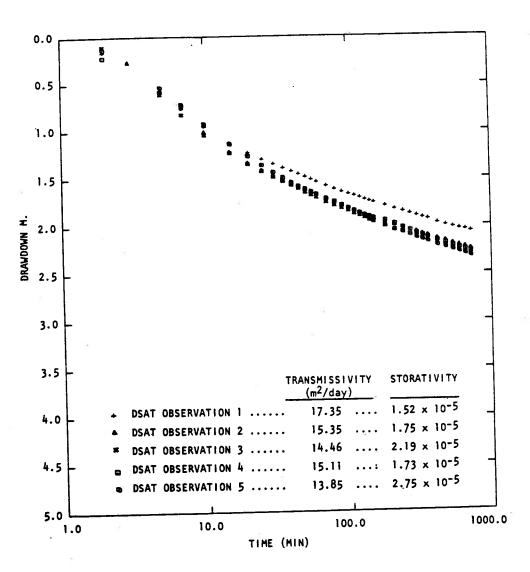


Fig. 6d Composite drawdown plots for DSAT observation well

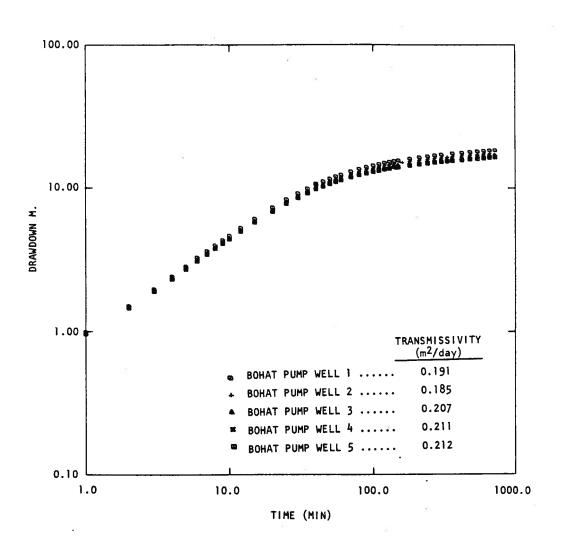
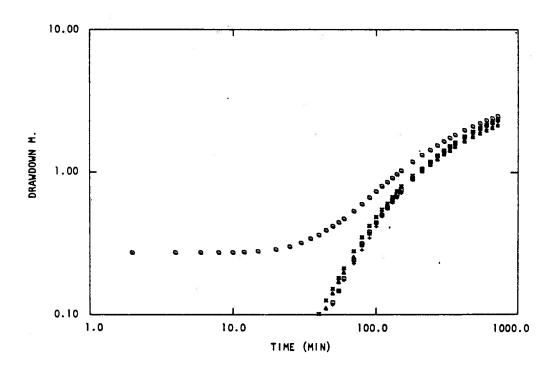


Fig. 6e Composite drawdown plots for BOHAT pumping well



						TRANSMISSI (m ² /day	STORATIVITY
	=	BOHAT	OBSERVATION	1		0.711	 5.88×10^{-4}
	•		OBSERVATION			_	6.06×10^{-4}
•	•	BOHAT	OBSERVATION	3	,	0.850	 4.01×10^{-4}
	+	BOHAT	OBSERVATION	4		0.667	 6.66×10^{-4}
	•	BOHAT	OBSERVATION	5		0.717	 6.30×10^{-4}

Fig. 6f Composite drawdown plots for BOHAT observation well

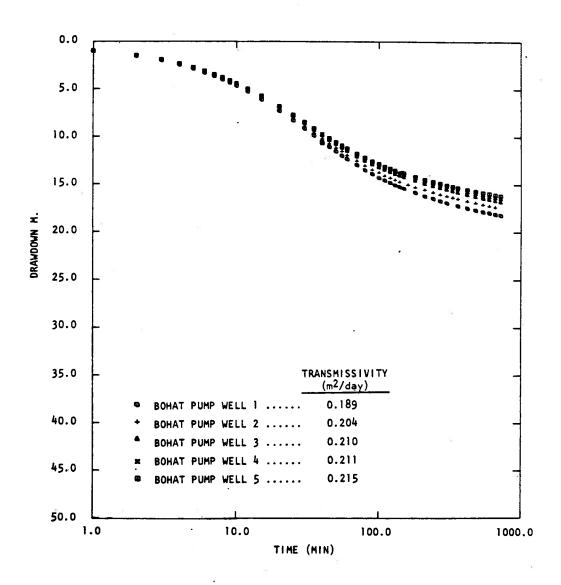


Fig. 6g Composite drawdown plots for BOHAT pumping well

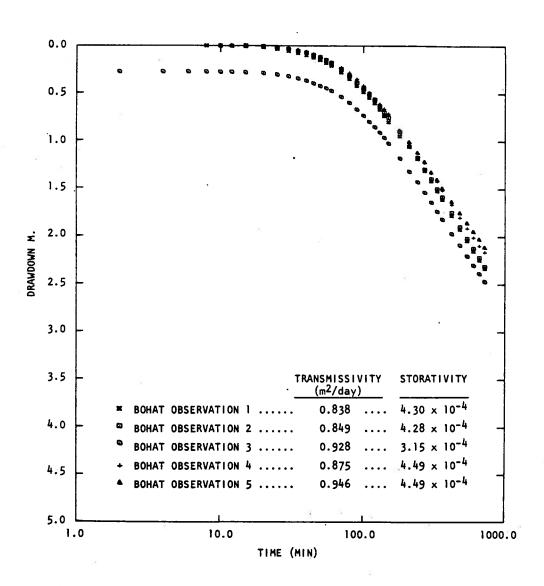


Fig. 6h Composite drawdown plots for BOHAT observation well

gravel aquifer had an average transmissivity of 17.7 square meters per day (m²/day) and a storativity of about 1.4 x 10⁻⁵. In addition time-drawdown plots for both the pumping and observation wells showed effects (beginning approximately at 200 minutes) which suggest either leakage or the presence of a recharge boundary. Leakage is the more probable explanation because during DSAT 1 water levels in the bedrock wells also responded to pumping. There are three possible causes for this leakage; (1) poor casing seals, (2) the fact that the two drift wells were drilled 0.3 m into the bedrock, or (3) that interformational leakage was occurring. The presence of this leakage, however, did not complicate the analysis of the data as aquifer parameters were calculated before leakage

The analysis of data from observation well BSC during aquifer performance test BOHAT 1 indicated that the bedrock "aquifer" had an average transmissivity of $0.78 \text{ m}^2/\text{day}$ and a storativity of about 5×10^{-5} (Table 3). During this test, leakage effects were evident in the pumping well after 100 minutes but were seemingly not present in the observation well data. This would indicate that the leakage was occurring only in the vicinity of the pumping well and not areally into the bedrock aquifer. Another interesting feature of this leakage

Table 3. Results of Bedrock Aquifer Performance Tests - New Norway Seismic Project

	Pumpi	ng Wel	(Well	вон)	0	bservation Wel	1 (Well	BSC)
	Straight Line		t Type Straight Curve Line		•	Type Curve		
	Ţ	S	T	S	T	S	T	S
BOHAT 1	0.189		0.191		0.838	4.30 × 10 ⁻⁴	0.711	5.88 x 10 ⁻⁴
BOHAT 2	0.204		0.185		0.849	4.28×10^{-4}	0.652	6.06×10^{-4}
BOHAT 3	0.210		0.207		0.928	3.15×10^{-4}	0.850	4.01×10^{-4}
BOHAT 4	0.211		0.211		0.875	4.49×10^{-4}	0.667	6.66×10^{-4}
BOHAT 5	0.215		0.212		0.946	4.49×10^{-4}	0.717	6.3×10^{-4}

 $T = Transmissivity (m^2/day)$

S = Storativity

was that it began when the water level in the pumping well was approximately 24 m below ground surface or at bedrock-drift contact. Leakage along the casing or conversion from confined to unconfined conditions are possible explanations. As with the drift test, however, analysis of aquifer parameters of the bedrock was not complicated by this effect.

Well Characteristics

Pre-detonation well characteristics were evaluated using well performance tests, BSCWT 1, BOHWT 1, and DSWT 1. No well performance tests were completed using well DN. Basically, the purpose of the well performance tests was to calculate the aquifer loss constant, B, and well loss constant, C, in the equation:

$$s = BQ + CQ^P$$

Where

s = drawdown in the well (m);

- B = aquifer or formation loss constant (head loss due to laminar flow); usually assumed to be caused by the aquifer; this term also includes laminar well losses which are not usually separable from the aquifer losses (meters per m3/day);
- C = well loss constant (head loss occurring due to turbulent flow),
 usually caused by well construction (meters per m⁶/day²)
- P = exponent which indicates the severity of the turbulence;
- Q = discharge of the well (m3/day).

The metric units used for these parameters in this report are shown in parentheses. In addition to evaluating the above parameters by the three methods mentioned, well efficiencies at the end of each well performance test were also calculated using the formula:

Well efficiency =
$$\frac{BQ}{BQ + CQ^2} \times 100$$

Because of the testing sequence required there was usually not enough time between well performance tests to allow complete recovery of water levels. This meant, especially for the BSC well tests, that water levels were recovering steeply at the start of the testing. Because it was felt that this recovery may have a significant effect on the calculated parameters, an attempt

was made to correct drawdown readings. Ultimately this was not necessary as the increase in drawdown which could be attributed to the recovering water level trend was less than one percent of the total drawdown caused.

Table 4 shows, inter alia, pre-detonation values of B, C, P, and well efficiencies. Figures 7a to 7f show the methods of calculation of these parameters for the first and last well performance test of each well. Poor data from BSCWT 1 during the first and last steps necessitated using data from the middle three steps of this test. As expected, efficiencies for well DS were slightly lower than the bedrock wells indicating a higher turbulent is we component due to the slotted casing completion at the high pumping rates. I irect comparisons of B and C calculated from BSCWT 1 and BOHWT 1 indicate that these parameters were similar for both wells. The slotted casing completion in well BSC, probably because of the very low pumping rates, did not, therefore, markedly affect turbulent flow components. Well DS, on the other hand, had well effects (CQ²) which caused a higher percentage of the total drawdown thereby lowering well efficiency.

Using, as example, the results of the Sheahan type curve method gives the following equations for pre-detonation well characteristics after 500 minutes of pumping:

Well BSC: $s = 1.15Q + (4.6 \times 10^{-2}) Q^2$

Well BOH: $s = 0.96Q + (3.3 \times 10^{-2}) Q^2$

Well DS: $s = 0.054Q + (5.4 \times 10^{-4}) Q^2$

Groundwater Quality

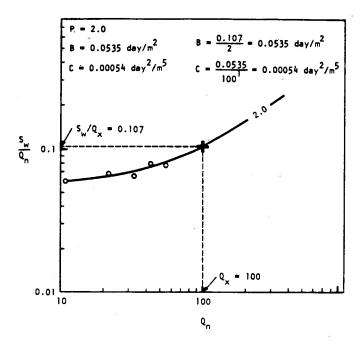
Water samples were collected at the beginning and near the end of the predetonation aquifer and well performance tests (App. D and Figs. 8a to 8e). Both the drift and bedrock groundwaters were of poor quality with total dissolved solids concentrations of 1400 to 1700 mg/l. The drift groundwater was a calcium-sodium-sulfate-bicarbonate type and had high concentrations of alkalinity, hardness, sulfate, bicarbonate, and iron. The bedrock groundwater was similar, being a sodium bicarbonate-sulfate type of slightly better quality

Table 4. Results of Well Performance Tests - New Norway Seismic Project

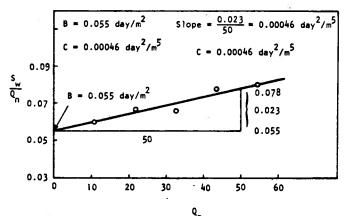
	Sheahan (1971)			Bierschenk & Wilson (1961)			Labadie & Helweg (1975)			Well Efficiency after 500 Mins. (%)		
Test Number	В	С	P	В	С	P*	В	С	Р	Sheahan	Bierschenk Wilson	Labadie Helweg
BSCWT 1	1.15	0.046	2.0	1.23	0.036	2.0	0.600	0.601	1.20	77	82	40
BSCWT 2	1.20	0.03	2.0	1.26	0.024	2.0	1.33	0.004	2.66	79	82	87
BSCWT 3	1.16	0.026	2.0	1.22	0.024	2.0	1.176	0.047	1.79	75	79	76
BSCWT 4	1.175	0.027	2.0	1.15	0.031	2.0	1.123	0.061	1.74	76	75	73
BSCWT 5	1.16	0.026	2.0	1.18	0.027	2.0	1.289	0.0018	2.91	75	76	83
DSWT 1	0.054	0.00054	2.0	0.055	0.00046	2.0	0.0534	0.0004	2.04	68	69	67
DSWT 2	0.050	0.00052	2.0	0.052	0.00043	2.0	0.0426	0.0032	1.59	67	69	57
DSWT 3	0.047	0.00053	2.0	0.047	0.00051	2.0	0.0239	0.01	1.41	63	63	32
DSWT 4	0.043	0.00057	2.0	0.044	0.00056	2.0	0.0376	0.002	1.72	59	60	51
DSWT 5	0.049	0.00054	2.0	0.051	0.0005	2.0	0.0489	0.0003	2.13	62	65	62
BOHWT 1	0.96	0.033	2.0	1.055	0.026	2.0	1.0284	0.0525	1.76	68	, 75	73
BOHWT 2	0.99	0.032	2.0	1.06	0.026	2.0	1.07	0.017	2.16	70	75	72
BOHWT 3	0.99	0.027	2.0	1.005	0.025	2.0	0.8321	0.1101	1.59	74	75	62
BOHWT 4	1.065	0.023	2.0	1.05	0.027	2.0	1.1152	0.0179	2.04	77	76	80
BOHWT 5	0.81	0.0404	2.0	0.80	0.04	2.0	0.77	0.0715	1.78	62	61	58

^{*} P is assumed as 2.0 in this method

DSWT I Q = 10.9, 21.8, 32.7, 43.6, 54.5 m³/day SHEAHAN ANALYSIS



BIERSCHENK AND WILSON ANALYSIS

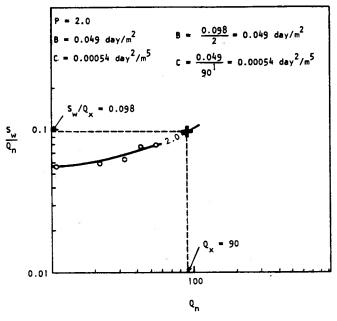


LABADIE AND HELWEG ANALYSIS

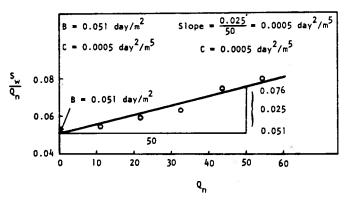
Q	SW	OPTIMAL P = 2.0430
10.900	0.650	B = 0.0534
21.800	1.430	C = 0.0004
32.700	2.145	MIN.ERROR = 0.0289
43.600	3.370	
54.500	4.350	

Fig. 7a Analysis of well performance test DSWT 1

DSWT 5 Q - 10.9, 21.8, 32.7, 43.6, 54.5 m³/day SHEAHAN ANALYSIS



BIERSCHENK AND WILSON ANALYSIS

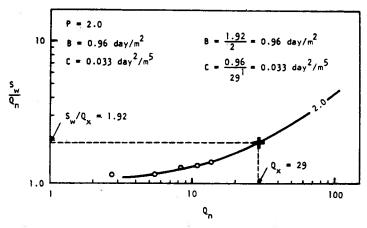


LABADIE AND HELWEG ANALYSIS

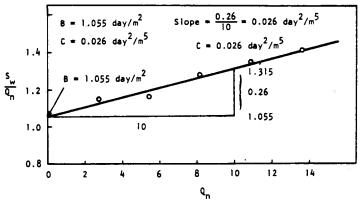
Q	SW	OPTIMAL P = 2.1300
10.900	0.610	B = 0.0489
. 21.800	1.315	c = 0.0003
32.700	2.063	MIN.ERROR = 0.0171
43.600	3.240	
54.500	4.280	

Fig. 7b Analysis of well performance test DSWT 5

BOHWT 1 Q = 2.725, 5.45, 8.175, 10.9, 13.625 m³/day SHEAHAN ANALYSIS



BIERSCHENK AND WILSON ANALYSIS



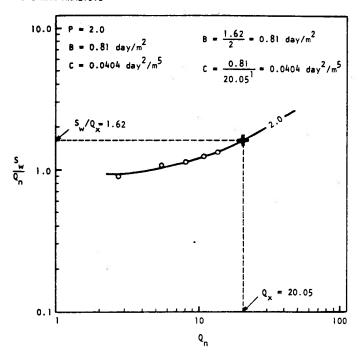
LABADIE AND HELWEG ANALYSIS

Q	SW	OPTIMAL P = 1.7590
2.725	3.140	B = 1.0284
5.450	6.640	C = 0.0525
8.175	10.430	MIN.ERROR = 0.0234
10.900	14.830	
13.625	· 19.170	

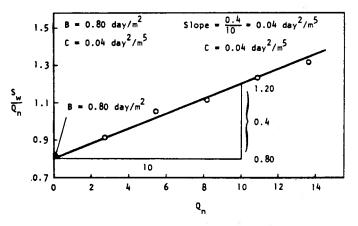
Fig. 7c Analysis of well performance test BOHWT 1

BOHWT 5 Q = 2.725, 5.45, 8.175, 10.9, $13.625 \text{ m}^3/\text{day}$

SHEAHAN ANALYSIS



BIERSCHENK AND WILSON ANALYSIS



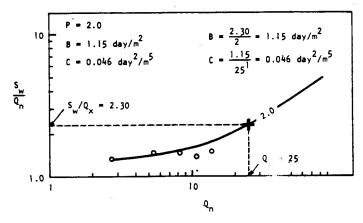
LABADIE AND HELWEG ANALYSIS

Q	SW	OPTIMAL P = 1.7790
2.725	2.490	B = 0.7704
5.450	5.750	c = 0.0715
8.175	9.190	MIN.ERROR = 0.0267
10.900	13.475	
13.625	17.935	

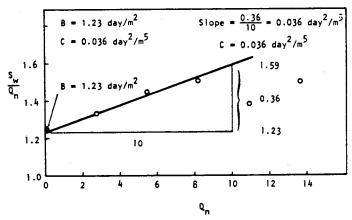
Fig. 7d Analysis of well performance test BOHWT 5

BSCWT 1 Q = 2.725, 5.45, 8.175, 10.9, 13.625 m³/day

SHEAHAN ANALYSIS



BIERSCHENK AND WILSON ANALYSIS



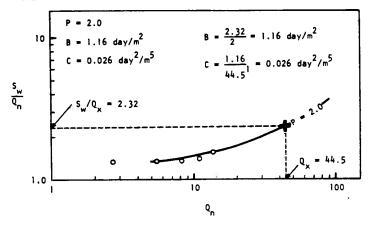
LABADIE AND HELWEG ANALYSIS

Q	SW	OPTIMAL P = 1.1980
2.725	3.636	B = 0.6009
5.450	7.860	c = 0.6014
8.175	12.365	MIN.ERROR = 0.0000

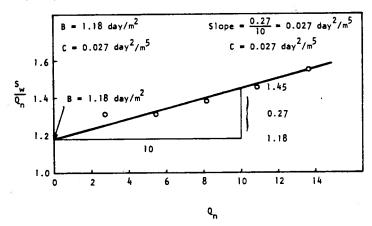
Fig. 7e Analysis of well performance test BSCWT 1

BSCWT 5 Q = 2.725, 5.45, 8.175, 10.9, 13.625 m³/day

SHEAHAN ANALYSIS



BIERSCHENK AND WILSON ANALYSIS



LABADIE AND HELWEG ANALYSIS

OPTIMAL P = 2.9070	SW "	- Q
B = 1.2890	3.585	2.725
c = 0.0018	7.220	5.450
MIN.ERROR- = 0.0050	11.365	8.175
	15.885	10.900
	21.085	13.625

Fig 7f Analysis of well performance test BSCWT 5

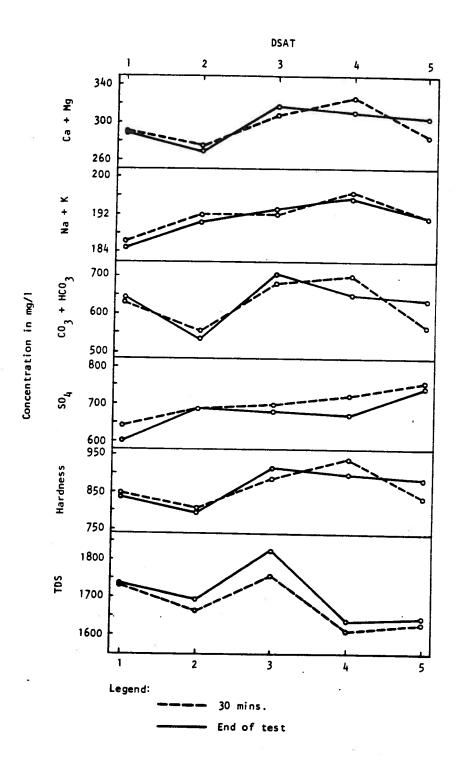


Fig. 8a Chemical variations during DSAT

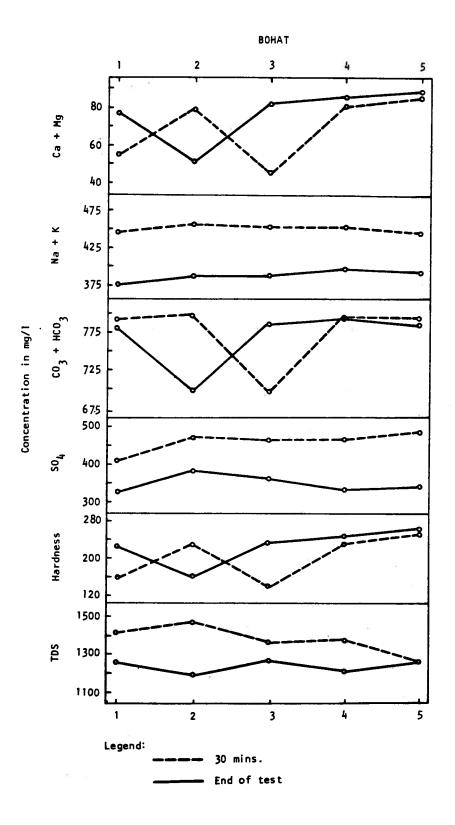


Fig. 8b Chemical variations during BOHAT

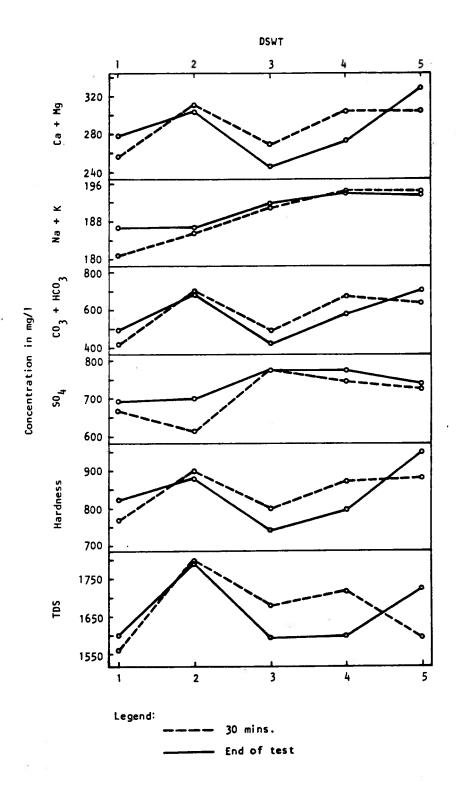


Fig. 8c Chemical variations during DSWT

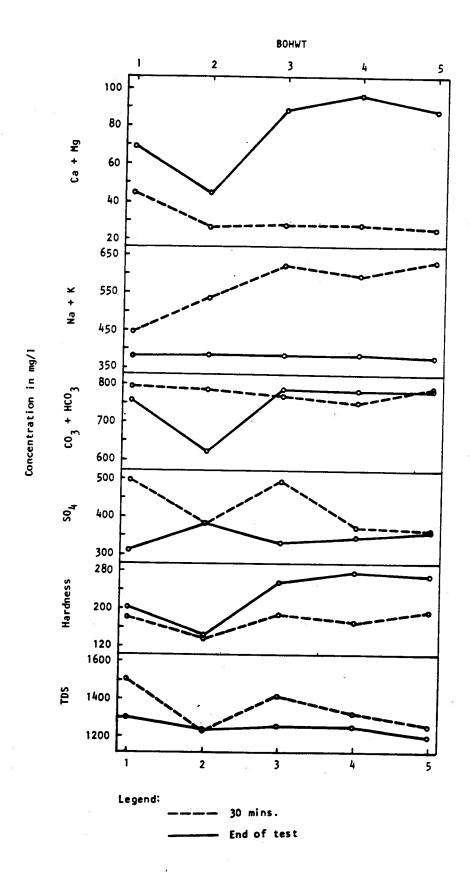


Fig. 8d Chemical variations during BOHWT

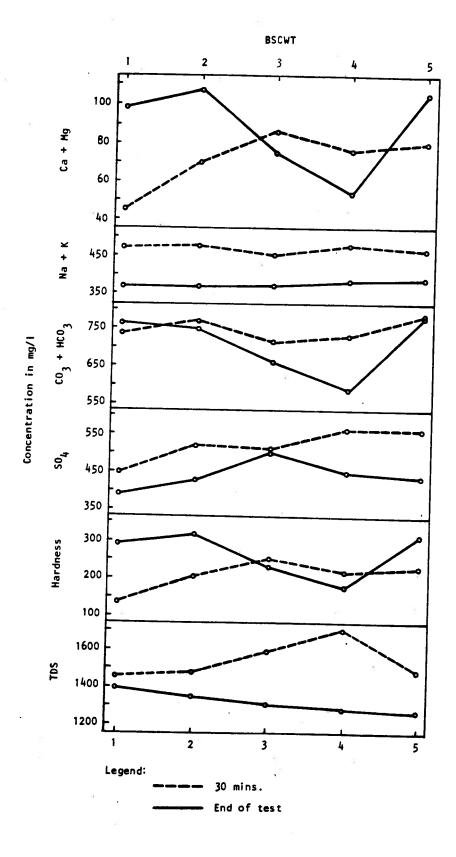


Fig. 8e Chemical variations during BSCWT

with high concentrations of alkalinity, hardness, sulfate, bicarbonate, and iron. Groundwater temperatures for both aquifers were in the range 5°C to 7°C.

Water Level fluctuations

Figure 5 shows water level fluctuations for all wells at the project site. All aquifers were responsive to changes in atmospheric pressure because of the confined groundwater conditions. Static water level fluctuations generally occurred between 8 and 9 m below ground surface for both aquifers, with the bedrock aquifers exhibiting the largest fluctuations during the pre-detonation period.

POST-DETONATION HYDROGEOLOGICAL CHARACTERISTICS

Aquifer Characteristics

Post-detonation aquifer characteristics were evaluated by means of aquifer performance tests BOHAT 2 to BOHAT 5 and DSAT 2 to DSAT 5 (App. C, Tables 2 and 3). In addition, composite time drawdown plots of all (including pre-detonation) aquifer performance tests are shown in figures 6a to 6h.

For the drift aquifer, analysis of the time-drawdown data for the observation well indicates that for post-detonation conditions, the transmissivity ranges between 13.85 and 16.18 m²/day and the storativity between 1.16 x 10^{-5} and 2.75×10^{-5} . These values are in excellent agreement with pre-detonation values (Table 2) and indicate that, within the limits of experimental error, the transmissivity and storativity of the drift aquifer were not changed by shothole detonations. This can be seen graphically in figures 6a to 6d, the composite time-drawdown plots, where data from all DSAT tests are extremely similar. One could argue that since the pre-detonation transmissivity average for DSAT 1 observation well is 17.53 m²/day and the post-detonation values of transmissivity average 15.4 m²/day, transmissivity has been decreased by 12 percent because of the shothole detonation. This variation, however, is probably due to experimental error, especially since there were four post-detonation tests compared to one pre-detonation test. Besides, a variation

in transmissivity of this magnitude would not really form the basis of a claim for a damaged water well due to aquifer damage. The effects of leakage, mentioned under pre-detonation drift aquifer testing, were also present during all post-detonation drift aquifer testing. As previously mentioned, the effects of this leakage did not complicate the calculation of aquifer parameters.

Bedrock aquifer performance tests basically substantiate the above findings. Analysis of time-drawdown data for the observation well (well BSC) indicated that post-detonation aquifer transmissivities ranged from 13.85 to $16.18 \text{ m}^2/\text{day}$ and the storativity from 3.15×10^{-4} to 6.66×10^{-4} . Once again, these values were in excellent agreement with pre-detonation values and table 3 summarizes the results of BOHAT 2 to BOHAT 5. Composite plots of the observation well data (Figs. 6a-6h) indicate the relatively constant transmissivity and storativity values of the bedrock aquifer before, during and after the shothole detonations. In this case, however, the aquifer transmissivity, strictly interpreted, shows a five percent increase during post-detonation testing. This variation in transmissivity is certainly possible considering the analytical methods employed and therefore should not be construed as an indicator of well development or an effect caused by shothole detonation. The leakage or conversion effect, mentioned under pre-detonation testing, was consistently obvious during post-detonation testing.

Well Characteristics

Post-detonation well characteristics were evaluated using tests BSCWT 2 to 5, BOHWT 2 to 5, and DSWT 2 to 5. Semi-log plots of these tests are shown in appendix C, typical analyses are shown in figures 7a to 7f and table 4 summarizes the results obtained.

During the post-detonation period, the values of B and C, for individual wells, remained relatively constant using the three methods of analysis. There is no evidence which suggests that shothole detonation has effected laminar or turbulent flow components of drawdown in any particular well. A slow decline in the efficiency of well DS can be attributed to a gradual loss in total depth because of

sand entering the well. As during the pre-detonation period, the efficiency of well DS is slightly lower than the bedrock wells because the turbulent component of flow forms a larger component of drawdown. In comparing B and C values of the two bedrock wells, turbulent flow components (CQ²) for each well are similar, suggesting that the slotted casing completion did not affect efficiency because of the low pumping rates. The aquifer loss constant, however, averages 20 percent higher for well BSC. This is a result of the drawdown in well BSC being greater than that in well BOH during well performance tests. As the aquifer loss constant affects the drawdown caused by laminar flow (both from the aquifer and the well) this higher value may indicate that the slotted casing completion affected laminar rather than turbulent flow components at low pumping rates.

Examination of wells after each detonation, using the down-the-hole camera, did not indicate any visual damage to wells or aquifers.

Groundwater Quality

Groundwater samples were collected during all post-detonation aquifer and well performance tests and analyzed for standard cations and anions (App. D). The variations in groundwater quality (Figs. 8a to 8e) can basically be examined in two ways: vertically, which shows the relationship between water quality at the start and end of a test; and horizontally, which shows any chemical trends during the post-detonation testing sequences.

Examining figures 8a to 8e, in a vertical sense, indicates that there was a definite interaction, in the form of leakage, between the drift and the bedrock aquifers. Because of the large differences in transmissivity, however, the chemical effects of this vertical movement of groundwater can be more easily recognized during the bedrock tests because the leakage formed a much larger component of total flow to the well and thus affected the groundwater chemistry of the bedrock aquifer to a greater degree. For example, most bedrock groundwaters increased in Ca+Mg concentration during testing which probably indicated movement of drift groundwaters (which are higher in Ca+Mg) into the bedrock via poor casing seals or interformational leakage. Accompanying this increase in Ca+Mg was a

decrease in Na+K, and a slight increase in sulfate. Reversals (especially in BOHAT — figure 8b) in Ca+Mg and CO_3 +HCO3, between the beginning and the end of a particular test are due to the precipitation of CaCO3 in the groundwater sample. The groundwater chemistry of the drift aquifer was also affected, to a lesser degree, by this leakage. Although the changes in concentrations were not as large as for the bedrock, Ca+Mg concentrations generally decreased while Na+K and CO_3 +HCO3 generally increased.

Over the period of post-detonation testing (Figs. 8a to 8e) it is difficult to ascertain any striking trends in water quality caused by shothole detonation. Both the drift and bedrock groundwater showed the favorable trend of a gradual decrease in total dissolved solids. For the bedrock groundwater, most other constituents, although varying considerably over the post-detonation period, had final concentrations which were very similar to the initial pre-detonation values. Drift groundwaters showed a gradual increase in concentration of numerous constituents during the post-detonation period, viz. Ca+Mg, Na+K, and SO4. Although it is possible that these increases were caused by detonations it is more likely that increases in Ca+Mg and SO4 were caused by overlying drift (i.e. intertill sands and gravels) groundwaters and that the increase in Na+K was caused by contributions from the bedrock.

Water Level Fluctuations

The response of water levels during shothole detonations and well depths, taken after each detonation, are shown in figure 9. During shothole detonations wells were equipped with mechanical water level recorders which gave an insensitive but adequate record of the water level fluctuations caused by the detonations. As expected, the magnitude of water level response increased the closer the detonations were to the wells. The largest measured response, approximately 2.5 cm, occurred in well BOH during the final (4.6 m) shothole detonation. The water level fluctuation caused by the shothole detonation at 183 m was barely measurable with mechanical equipment (Fig. 9).

Well (Original	4.6m shot Dec 12,1978 10:50 AM	15m shot Dec 5,1978 10:27 AM	61m shot Nov 28, 1978 10:32 AM	183m shot Nov 21,1978 10:45 AM
well depth, m)	(Well depth,m,after shot)	=		(Well depth,m,after shot)
	10:40 AM 11:10 AM	10:15 AM 10:45 AM	10:15 AM 10:45 AM	10:30 AM 11:00 AM
	8.825 -	8.82 ~	8.82 -	8.835 -
DN (26.2m)	8.84 -	8.835 —	8.835 -	8.85
	8.855 -	8.85 -	8.85 —	8.865 -
	(26.30m)	(26.305m)	(Not taken)	(26.30m)
	8.835 -	9.57 -		9.96 -
BOH (73.15m)	8.85	9.585 -	No chart	9.975 -
	8.865 - (58.77m)	9.60 - (58.80m)	(Not taken)	9.99 - (58.84m)
	9.87 -	08:57 AM 11:57 AM 9.91 -	9.915-	9.955 -
- BSC (73.15m)	9.885	9.925 -	9.93 -	9.97 -
	9.90 – (72.87m)	9.94 - (72.86m)	9.945 (Not taken)	9.985 - (72.90m)
DS (25.30m)	No chart	No chart	No chart	No chart
	(23.48m)	(23.765m)	(Not taken)	(24.21m)

Fig. 9 Water level fluctuations during detonations

Figure 5 shows the water level fluctuations before, during, and after aquifer and well performance tests. Because smaller transmissivities caused greater drawdowns, the bedrock aquifers showed the greatest range in fluctuations during testing. Figure 5 also indicates that during the post-testing period, potentiometric surfaces returned to pre-testing levels, indicating that shothole detonations had not significantly altered static water levels in the wells. A plot of

barometric pressure versus post-testing water levels (Fig. 10) indicates the bedrock and drift aquifers maintained their responsiveness to barometric pressure fluctuations.

The shapes of the water level response curves shown in figure 9 indicate the qualitative transmissivity of each aquifer type. The drift aquifer responded and recovered much more quickly than the bedrock, indicating the effect of its larger transmissivity. Although it was expected that detonation would cause an initial compression of the aquifer, and thereby induce a rise in water level, this is not consistently obvious (Fig. 9). In most cases, the initial (and sometimes only) response is downward indicating a dilation of the aquifer. Although the mechanics of the observed response are not fully understood, it is probable that the recording equipment employed was not sensitive enough to record the complete response sequence. For example, when comparing responses for well DN, it is clear that they differ for the 4.6 m and 15 m detonations. During the 15 m detonation the initial reaction of the aquifer is one of dilation followed by a recovery of water level. During the 4.6 m detonation, however, the aquifer seemed to be solely in compression and it is possible that the initial dilation was not detected by the recording equipment. Another interesting observation is that the slotted casing completion of well BSC seemed to dampen the magnitude of water level response to detonation when compared with well BOH. Admittedly, well BOH was closer to the detonations but this is really only a factor for the last detonation. During the 15 m detonation, for example, actual radial distance from detonation to well BOH was 17 m and to well BSC was 27 m, yet water levels in well BOH responded with a magnitude 3 to 4 times that of well BSC. If this is generally the case, the effects of seismic detonations may cause significantly less water level responses in wells completed with slotted casing.

As mentioned, the mechanics of the water level responses during detonations are not fully understood. Overall, however, the fact that the detonations did not have large effects on water levels in the wells was the more important result.

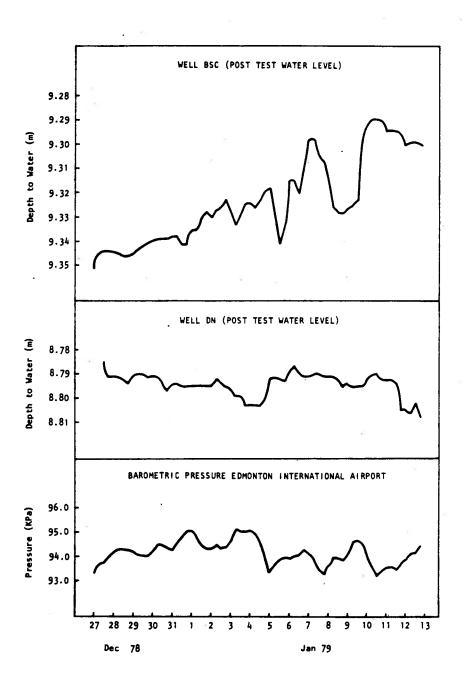


Fig. 10 Post-testing water level fluctuations

CONCLUSIONS

Conclusions from the present study are stated with recognition that the set of aquifer and well conditions encountered and tested at the project site are unique to certain geologic and hydrogeologic areas of the province. In this respect, the results of the study are limited in their applicability and it would be dangerous to apply the results of this project to all areas of the province and make broad generalizations about the effects of seismic detonations on water wells. It is felt, however, that in areas of similar geologic and hydrogeologic conditions, the results of this study will prove useful in evaluating future claims. The fact that the well drilling and construction methods used were very similar to standard methods of constructing domestic water wells in Alberta adds validity to the results. Hopefully, a continuation of similar projects will allow a complete coverage of the aquifer and well types in Alberta.

Some readers may be tempted to criticise the validity of the results of this study because the shotholes were not completed in the bedrock as is normal in petroleum exploration techniques. This may have caused the low velocity drift aquifer to act as a sponge and dampen the effect of the detonations on the bedrock wells. It should be remembered, however, that the objective of this project was to determine any effects of shothole detonations on both the drift and bedrock wells. Considering the well and shothole configuration at New Norway, well DS was the closest well, both horizontally and vertically, to the detonations. Therefore a detonation less than 6 m away, would have had maximum effect on this well and lesser effects on more distant wells. Since well DS remained unaffected by shothole detonations, it would seem that the results of this project are valid.

It would seem timely and practical to concentrate on those parameters which are commonly in question or need evaluation in seismic detonation-water well claims. These are understood to include:

- Well and aquifer characteristics e.g. increased drawdowns, no water in well, higher pumping lifts.
- Well yield and depth e.g. well doesn't pump as much, increased sand, well caved, loss of depth.

- 3. Water quality e.g. bad taste, bad smell, water cloudy.
- 4. 4. Water levels e.g. drastic fall or rise in water level.

Well and Aquifer Characteristics

Extensive testing (of the aquifers and wells) at the New Norway site indicate that the seismic detonations had little or no effect on the aquifer and well characteristics. Pre-detonation and post-detonation values of transmissivity, storativity, aquifer losses, well losses and well efficiency were basically in excellent agreement. Minor changes, in these parameters, did occur but in a fashion suggestive of experimental error rather than detonation induced changes. The down-the-hole camera did not indicate any specific damage to any water well at the site. Based on the results of this study it would be difficult, in areas of similar conditions, to entertain the suggestion that seismic detonations had increased drawdowns in wells. Composite time-drawdown plots confirm these findings.

Well Yield and Depth

Seismic detonations, because they did not affect aquifer or well characteristics, did not affect the yield of any well at the site. Aquifer and well performance tests were conducted at exactly the same pumping rates, before and after detonations, with similar pumping water levels. The two wells which showed a significant loss of depth were wells BOH and DS. Well BOH bridged at 59 m before detonations took place, presumably because of unstable hole conditions. Because of the slotted casing completion of well DS, fine sand was continuously entering the well during testing which caused a gradual loss in depth. Loss of depth, well caving or loss of production did not occur in any wells during detonations.

Water Quality

Variations in groundwater quality during testing were mainly attributable to the aquifer conditions encountered. Although many chemical constituents varied during the post-detonation period, the final post-detonation values were similar to pre-detonation values. Most trends observed during the post-detonation period were due to groundwater leaking vertically between aquifers. The down-the-hole camera indicated that groundwater in the wells was slightly turbid immediately after a detonation, but this condition disappeared after one or two minutes at the beginning of the subsequent pumping test. No chemical changes in groundwater chemistry at the site can be directly attributed to detonations.

Water Level Fluctuations

Observation of water level records show that from a distance of five meters a shothole detonation caused a maximum measured water level fluctuation in well BOH of approximately 2.5 cms. Generally, the water level response recorded during the detonation did not conform to the theory that the first effect of a detonation on an aquifer should be compression thereby causing a rise in water levels. This is attributable to the lack of sensitivity of the measuring devices used. The effects of the detonation 183 m from the wells was barely measurable and in general the shothole detonations had only minor effects on the water levels in the wells. There is an indication that slotted casing completion tends to dampen water level fluctuations caused by detonations.

RECOMMENDATIONS

- 1. It is strongly recommended that these seismic detonation-water well evaluations be continued in different geologic and hydrogeologic areas of Alberta using the same scientific methodology as the New Norway project. In this way, a set of studies can be produced which will ultimately be applicable for all areas of Alberta. It is suggested that the next site be located in an area where fractured coal seams are important domestic aquifers.
- 2. A number of scientific improvements and changes could be recommended for the next project. A more sensitive water level measuring device using a pressure transducer, for instance, should be used during detonations. Such a unit is presently being built by the Groundwater Division, Alberta Research Council. Monitoring of pre-detonation groundwater chemistry should take

place over a longer time before testing begins. This would allow a more accurate evaluation of the natural variations in the concentrations of the main chemical constituents. For the sake of completeness, the next project should have one well completed with a well screen.

3. It would be instructive at the New Norway site to deepen existing shotholes and repeat the project. It is possible that the occurrence of a highly transmissive drift aquifer vertically between the detonation and the bedrock may have had a buffering effect. It has to be decided whether this procedure would have priority over a new project site.

ACKNOWLEDGEMENTS

The following Groundwater Division personnel were involved in the project and report preparation and the author gratefully acknowledges their help:

Origination of scope and basic methodology of the project - G. Gabert

Fieldwork - G. Sjostrom and H. Özbey

Data Compilation - A. Beerwald

Photo credits - W. Ceroici

Organization of report - M. Madunicky

Draughting - M. Madunicky and P. Politzer

Typing - B. Brown, M. Flanagan and J. Probert

Critical review of manuscript - G. Gabert, D. Hackbarth and J. Tóth.

Alberta Environment graciously supplied the down-the-hole camera and operator.

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Appendix A

ORIGINAL PROJECT PROPOSAL EXPLORATION AND PROJECT SITE DRILLING

This appendix has been transcribed from field notes. Units are therefore in feet or gallons except where shown.



The 4.6 m shothole detonation. Continuous water level recorder shown in background. This photo was taken a few seconds after the cover photo.

A Proposed Study

EVALUATION OF THE EFFECTS OF SEISMIC EXPLOSIONS IN SHOTHOLES ON WATER WELLS AND AQUIFERS

OBJECTIVES

The primary objective of the program is to evaluate the effects of seismic explosions in shotholes on water wells and aquifers typically found in Alberta. A secondary objective is to establish distances at which seismic explosions in shotholes should be conducted away from water wells in order to minimize or eliminate damaging effects.

SCOPE

The study will be limited initially to one site which will be selected on the basis of being a typical Alberta Plains environment in respect of aquifer occurrence and geology. A minimum of four water wells will be completed at the site and the aquifer and well conditions evaluated. Explosive charges will be detonated at separate times in each of three shotholes located at specified distances from the wells. Well and aquifer conditions will be reevaluated after each particular explosion.

METHODS

Four water wells will be completed at the site; two shallow wells in an aquifer in surficial deposits (sand or gravel) and two deeper wells in a bedrock aquifer (sandstone). Water wells will be completed by the slotted casing and open hole methods which are commonly used in Alberta. Two wells will be completed with slotted casing in the aquifer in surficial deposits and two wells will be completed in the aquifer in bedrock; one well with slotted casing and the other open hole.

Maximum depths of wells in bedrock are planned to be not greater than 200 ft. The minimum distance between wells at the site will be 100 ft.

- 3. Complete two wells in the bedrock (sandstone); one with slotted casing and one open hole.
- 4. Measure "static" water levels.
- 5. Conduct an aquifer test in the surficial aquifer and the bedrock aquifer.
- 6. Obtain groundwater samples and water temperatures.
- 7. Conduct well tests in one well completed in the surficial aquifer and each of the two wells completed in bedrock deposits.
- 8. Drill three shotholes to 60 ft in depth; at distances of 600, 200 and 50 ft from the nearest water well.
- 9. Detonate a 10-lb explosive charge in the shothole 600 ft from the nearest water well.
- 10. Repeat "static" water level measurements, aquifer tests, sampling of groundwater, measurement of water temperature and well tests.
- 11. Detonate 10-1b explosive charge in the shothole 200 ft from the nearest water well.
- 12. Repeat step 10 above.
- 13. Detonate an explosive charge in the shothole 50 ft from the nearest well.
- 15. Repeat step 10 above.

Information on the sequence and composition of rock types (stratigraphy) and observation of permeable intervals will be recorded during drilling of the wells. Lithologic samples and an electric log of each well will also be obtained. Upon completion of the wells an aquifer test will be conducted on the shallow wells using one as the production well and one as an observation well. Similarly, an aquifer test will also be conducted on the deeper bedrock wells using the open hole well as the production well and the one completed with slotted casing as the observation well. The aquifer tests will be of 12-hour duration. A well test will be conducted on one of the wells in surficial deposits and each of the two wells in bedrock deposits. The test will consist of 5 steps, each at a different pumping rate and continuing for a period of 100 minutes. Aquifer coefficients of transmissivity and storativity will be calculated from aquifer test data and well efficiencies will be calculated from well test data.

A 10 pound explosive charge will be detonated in a 60-foot shothole at distances of 600, 200 and 50 ft from the nearest water well. Following each seismic explosion; aquifer tests, well tests, measurement of "static" water levels and water sampling will be repeated. This procedure will result in eight aquifer tests and twelve well tests.

An explosive charge will be detonated in a shothole while one of the aquifer tests is in progress (probably the one following the 200-foot explosion). Water wells will be observed for any immediate effect resulting from the explosion.

SUMMARY OF PROCEDURE

- 1. Select site
- Complete two wells with slotted casing in an aquifer in the surficial deposits (sand or gravel aquifer).

COST ESTIMATES

1.	Completion of water wells: 600 ft @ \$15.00/ft (Private Contracter)	9,000.00
2.	Electric logging: 600 ft @ \$0.25/ft	150.00
3.	Aquifer tests: 96 hours @ \$25.00/hr	2,400.00
4.	Well tests: 75 hours @ \$25.00/hr (9-500 minute tests)	1,875.00
5.	Drilling of shotholes 3 hours @ \$25.00/hr (3 holes 60 ft in depth)	75.00
6.	Basic salaries (2 man-months @ \$18,725.00/annum)	3,120.00
7.	Overhead on basic salaries (60%)	1,872.00
8.	Miscellaneous items	1,000.00
	Total estimated cost	\$19,492.00

PROJECT SITE

WELL BSC (Bedrock, Slotted Casing)

Location: NW 14-45-22-W4M Date: Nov. 1, 1978

Owner: Norman Newsted Water Level: 9.63m (Nov. 3/78)

Driller: Schmidt Drilling Est. rate of Production: 2-3 igpm

(Airlift)

M.P. (Measuring Point): 0.50m agl

1	Drift	:		
0	-	2		Top soil, black, organic
2	-	25		Till, clay silty brown (tan) soft with some occasional pebbles and trace of coal chips
25	-	70		Lake clay, silty and sandy, grey, plastic, sticky, soft, impervious with some coal chips At 51-52' 12" coal seam with pebbles At 59-60' 12" sand and gravel layer
70	-	84		Gravel size up to 3-4" mostly chert granite, quartz
Ве	edroc	k		(water)
84	-	135		Sandstone, slightly, bentonitic, light grey-beige soft very fine grained alternating with shale layers multiple thin coal seams at 115-125' and hard spot at 124-125'
135		160		Shale dark grey, dark brown, brittle alternating with sandstone layers and coal carbonaceous at places
160	-	1 70		Sandstone (as previously described)
170	=	187		Shale (as above)
187	_	195		Sandstone with shale and siltstone light grey, medium grained
195	-	205		Shale greenish grey
205	-	215	77	Shale, dark grey carbonaceous dark brown
215	-	225		Sandstone (as above) at 218-219' coal
225	-	230		Siltstone with coal seams
230	-8	232		2 ft coal seam
232	=	235		Shale (as above)
235	-	240		Sands tone

PROJECT SITE

WELL BSC (Bedrock, Slotted Casing)

- Complete E-log
- 97 ft 5 1/2" Casing and 147 ft slotted casing installed in the hole
- It is a bedrock slotted casing hole (BSC)
- Est. 2-3 igpm production (airlift)

Water Level Measurements

Date		Time	Water Level	(m)
Nov.	3/78	8.45	9.63	
Nov.	7/78	8.45	9.38	
Nov.	7/78	12.00	9.57	

PROJECT SITE

WELL BOH (Bedrock Open Hole)

Loca	tion:	NW 14-45	5-22-W4M	Date: Oct. 30, 1978
0wne	r:	Norman .	lewsted	Water Level: 8.94m (Oct. 31)
Dril	ler:	Schmidt	Drilling	Est. rate of Production: 3-4 igpm (Airlift)
	n .c.			*
	Drift			
0	-	5	Clay till brown to tar 0-2 ft)	n, some coal (top soil at
5	-	26	Till, tan to brown cla	ay with some sand and pebbles
26	-	71	Lake clay, dark grey to occasional sand and pe	till, plastic minor coal with
71	-	83	Gravel size up to 3-4' quartzite granite	mostly consists of chert
Bed	drock		· ·	
83	-	85	Shale + salt and peppe grained	er sandstone grey, very fine
85	-	115	Sandstone light grey, bentonitic hard at 86- layers and some coal	salt and pepper slightly 95' alternating with shale
115	:=	120		carbonaceous brownish beige y light grey bentonitic
120	-	136	Sandstone, light to me very fine grained with	dium grey, slightly bentonitic, some shale layers
1 36	-	145	Shale, brown to brown (at 144' lost some wat	grey, relatively hard brittle er, sandstone)
145	i.=	152	Shale greenish grey	
152		158	Sandstone light grey,	very fine grained bentonitic
158	-	166	Carbonaceous shale, da	rk grey to brown
166	-	170	Sandstone (as previous	ly described)
170		176	Shale (as previously d	escribed)
176	-	177	Sandstone hard, lost s	ome water
177	-	215		rbedded, light grey - dark grey bentonitic layer, at 205-215
215	-	230	Carbonaceous shale + c	oal greenish grey to grey, brittle
230	-	231	12" coal seam	
231		240	Shale brown, beige to	dark brown, brittle

Bottom of Hole .

240

PROJECT SITE

WELL DN (Drift North)

Location:	NW 14-45	5-22-W4M	Date: November 2, 1978
Owner:	Norman N	lews ted	Water Level: 8.90m (Nov. 7/78)
Driller:	Schmidt	Drilling	Est. rate of production: 5-6 igpm (Airlift)
			M.P. (Measuring Point): 0.40m agl
Drift			
0 -	20	Till, silty clay, tan occasional pebbles and at 0-2 ft)	to brown, soft, sticky with trace of coal chips (top soil
20 -	73	Lake Clay, grey, plast sand, pebbles and grave 66 ft, boulder?	ic, sticky, impervious occasional els and coal chips hard spot at
73 -	85	Gravel sizes up to 3-4 quartz, granite fragmen	' mostly consists of chert, nts (Water)
Bedrock			
85 -	86	Sandstone - shale light bentonitic	t grey to dark grey, slightly
	86	Bottom of Hole	
	-	E-logged	
	-	Totally 87 1/2 (5 1/2"	size) casing installed in the hole
		0 - 74 blank casing 74 - 84 slotted casin 84 - 85 1/2 blank cas	ng sing

Water Level Measurements

<u>Date</u>	<u>Ti me</u>	Water Level	<u>(m</u>)
Nov. 7/78	8.40	8.90	
Nov. 8/78	12.00	8.81	

PROJECT SITE

WELL DS (Drift South)

Location:	NW 14-45-22-W4M	Date:	Oct.	31,	1978
Owner:	Norman Newsted	Water	Level	: 8	. 70 m

Driller: Schmidt Drilling Est. rate of Production: 5-6 igpm (Airlift)

M.P. (Measuring Point): 0.40m agl

[rift		
0	-	20	Till - tan to brown silty clay, soft sticky with occasional pebbles and trace of coal chips (Top soil at 0-2 ft)
20	-	72	Lake Clay sand, pebbles, gravels, and coal chips, sandy layer at 55-60 ft, more gravels at 65-72 ft
72	-	82	Gravel sizes up to 3-4" mostly chert, quartz and granite fragments (Water)
Bec	lrock		0.0
82	-	83	Shale - sandstone, grey salt and pepper slightly bentonitic
		83	Bottom of Hole
		-	E-logged the hole
		-	Totally 85 1/2 ft (5 1/2" size) casing installed in the hole (0-72' blank, 72-82 slotted and 82-84

blank casing)
Water sample taken

Water Level Measurements

Date	Time	Water Level	(m)
Nov. 2/78	8.45	8.68	
Nov. 3/78	8.45	8.70	
Nov. 7/78	-	8.70	

NEW NORWAY SEISMIC PROJECT EXPLORATION SITE I PILOT WELL #1 (Bedrock)

Location:

NW 17-44-21-W4M

Date: Oct. 17, 1978

Owner:

Eldon Graff

Driller:

Schmidt Drilling

	Drif		
	DELL	Ľ.	
0	7	10	Till - silty clay, brown grey mixture of silt, clay, sand boulders and coal chips
10	-	15	Silty clay grey, sandy, hard spot at 14' boulder
15	-	20	Silty clay grey, sandy, hard spot at 19' boulder some coal chips
20	-	25	Clay, grey
25	-	45	Clay, dark grey clayey, silty
45	-	52	Clay, dark grey clayey, silty at 45' hard spot aquifer
I	Bedro	:k	
52	-	60	Weathered sandstone, rusty buff colour at 52', very fine grain
60	-	70	Weathered sandtone, more sandy material, very fine grain
70	-	75	Weathered sandstone, more clayey material, very fine grain
75	-	80	Weathered sandstone, greyish brown, very fine grain
80	-	90	Sandstone - siltstone greenish grey to buff, very fine grain, layered, variegated
90	-	95	Sandstone-bluish grey very fine grain, shaley
95	_	105	Sandstone bentonitic, light grey-ash coloured
105	-	110	Shale, greenish grey with sandstone layers
110	-	115 .	Shale-sandstone, grey shale dominant with sandstone layers
115	_	120	Sandstone, bentonitic, very fine grained light grey, hard spots at 115 and 117'
120	-	150	Sandstone medium grey very fine grained
		150	Bottom of Hole

NEW NORWAY SEISMIC PROJECT EXPLORATION SITE 1 PILOT WELL #1 (Bedrock)

Hole E-logged

Water Level Measurements

<u>Time</u>	Water Level	(m)
13.30	10.00	
-13.36	10.00	
-13.40	10.00	
-13.50	9.96	
-14.00	9.91	
-14.10	9.88	
-14.20	9.86	
-14.30	9.84	
-14.30	9.81	
-14.40	9.81	
-15.03	9.81	

Estimated rate of Production Bedrock = 15.20 igpm (Airlift)

EXPLORATION SITE 3

PILOT WELL #3 BOH (Bedrock Open Hole)

Location: SE 25-44 (100 ft			-21-W4M south of Well-DN)	Date: Oct. 20, 1978	
Owner: Noah Toe		Noah Toe	ews	Est. rate of Production: 1-2 igpm?	
Driller: Schmidt		Schmidt	Drilling	(Airlift)	
Bit S	ize:		0-140.5 ft 142-260 ft		
D	rift				
0	-	15	Till, silt, brown sand	y and clayey with occasional	
15	-	20	Till, silt, brown, sand chips, with occasional	dy and clayey trace of coal boulders	
20	-	50	Silty clay, grey, very trace of coal chips	fine grain with sand and gravel,	
50	-	55	Silty clay, grey with o	coal seams	
55	-	85	Sand, clayey and silty multiple coal seams	, medium to coarse grain with	
85	in —	110	Gravel starts at 87' pe boulders up to 1-4" siz	ebbles quartz, chert, chunks of ze with coal chips	
110	-	115	Silty clay, grey, very at lll')	fine grain (end of gravel zone	
115	-	118	Silty clay, (as piece of light grey bentonitic	of sandstone starts at 118'	
Bedrock					
118	-	126	Sandstone light, grey, coal chips	bentonitic with plenty of	
126	-	131.5	Gravel coarse size up t	to 2" coal chips	
131.5	-	140	Sandstone with shale lavery fine grain bentoni	ayers, light grey to dark grey tic with coal seams	
140	-	165	Shale with sandstone ar siltstone, grey carbona	nd siltstone hard spot at 142' aceous with coal seams	
165	-	170		nd siltstone (12" coal seam at grey carbonaceous with coal seams	
170	-	180	Shale greenish grey-bei	ge, banded with siltstone	
180	-	190	Sandstone light grey, f bentonitic hard at 183	ine grain argillaceous, - 185' coal	
190	-	195	Shale dark brown		

NEW NORWAY SEISMIC PROJECT EXPLORATION SITE 2 PILOT WELL #1

Date: Oct. 17, 1978

Location: NW 25-44-21-W4M

Owner:		Noah Toe	Static Water Level: 2.22m	
Driller:		Schmidt	Drilling Est. rate of Production: 10 igpm (Airlift)	
	[Drift		
	0	- 2	10	Till silt, brown sandy, clayey with occasional boulders
7	10	- ,	15	Silty clay, grey with sand and boulders, coal chips
	15	-	20	Silty clay, grey with sand and 2" boulders, coal chips
	20	-	25	Silty clay, grey with sand and with boulders, coal chips
	25	-	35	Silty clay, grey with boulders
	Ве	drocl	‹	
	35	-	40	Sandstone-siltstone, hardspot at 36'
	40	-	50	Brown, grey very fine grain hard, brittle with coal chips
	50	-	55	Brown, coal seam at 52-53 1/2 feet
	55	-	60	Brown grey
	60	-	80	Brown grey medium grey
	80	-	85	Sandstone, bentonitic with coal seams light grey very fine grain
	85	-	95	Sandstone, bentonitic with coal seams medium hard
	95	-	100	Sandstone, bentonitic more coal
	100	-	115	Shale brown, dark grey with sandstone layers
	115	-	120	Sandstone medium grey very fine grain
	120	-	125	Coal seam and sandstone light grey, bentonitic very fine grain
	125	-	135	Sandstone with multiple coal seams grey medium grain
	135	-	140	Sandstone with multiple coal seams light grey bentonitic
	140	-	145	Sandstone with multiple coal seams
12	145	-	150	Sandstone hard sandstone at 147-149 feet

Hole E-logged

Bottom of Hole

150

NEW NORWAY SEISMIC PROJECT EXPLORATION SITE 1 PILOT WELL #2 (Drift)

NW 17-44-21-W4M Location:

Date: Oct. 17, 1978

Owner:

Eldon Graff

Est. rate of Production: 1.2 igpm
(Airlift)

Driller: Schmidt Drilling

0	-	15	Till, greyish brown mixture of sand, silt clay with some boulders and coal chips, very fine grained
15	-	25	Clay brown grey with some silt and sand
25	-	45	Clay brown dark grey very fine grain
45	-	50	Clay more sandy layers hard spot at 48' aquifer?
50	-	60	Weathered sandstone, rusty-buff very fine grain
60	-	65	Weathered sandstone, buff coloured
65	-	73	Weathered sandstone, buff coloured
		73	Bottom of Hole

NEW NORWAY SEISMIC PROJECT EXPLORATION SITE 3

PILOT WELL #3 BOH (Bedrock Open Hole)

195	-	200	Shale brown
200	() 	205	Sandstone medium hard fine grain light grey argillaceous, bentonitic
205	-	220	Sandstone medium hard fine grain with brown siltstone layers
220	-	225	Shale dark brown grey, with brown siltstone layers
225	-	260	Shale dark brown with sandstone layer at 250-252', light grey, bentonitic, some coal
		260	Total Depth of Hole
			4 1/2" casing installed to 140.5' and then driven to 142 ft, 1 1/2 ft into the shale
		3	(Oct. 23, 1978) Hole first drilled to 230 ft after E-logging reaming, casing installation and airlift tests (at 40' intervals decided to go deeper to 260' Estimated rate of production not more than 1-2 igpm (Airlift)

NEW NORWAY SEISMIC PROJECT EXPLORAT ON SITE 3 PILOT SITE #3

Location: SE-25-44-21-W4M

Date: Oct. 18, 1978

Owner:

Noah Toews

Drilling Started: 15.40

Driller:

Schmidt Drilling

Drilling Finished: 18.00

Water Level: 1.71m (Oct. 23/78)

	Drift	:	
0	-	20	Till, brown silt, clayey and sandy rock chips
20	-	25	Sandy silty clay, grey, with pebbles
25	-	40	Sandy silty clay, grey, with pebbles, trace of coal chips
40	-	65	Sandy clay, to medium grained grey, clayey with coal chips
65	-	80	Sandy clay (more sand) to medium grained grey, clayey with coal chips
80	- `	90	Sandy with clayey layers and coal chips
90	-	95	Sandy (more sandy layers) with clayey layers and coal chips
			Gravel Starts at 99 feet
99	-	116	Gravel quartz, felds, with trace of coal chips loosely cemented cobbles up to 2-3"
116	-	130	Sandstone, light grey, ash very fine grained argillaceous with occasional pebbles
130	-	134	Gravel (as of 99-116) very fine grained argillaceous
Bedrock		k	8
134	-	140	Sandstone grey, very fine grained, bentonitic

This well intended to be a bedrock slotted casing hole (BSC), reaming the hole from 4 1/2" to 6 3/4" to 120' 5 1/2" blank casing installed, drilling from 122' to 140' 5 1/8" RB. Because of 4 ft thick gravel found below the sandstone, casing removed hole abandoned.

E-logged

NEW NORWAY SEISMIC PROJECT EXPLORATION SITE 3

PILOT WELL #3 DN (Drift North)

Location: SE 25-44-21-W4M Date: Oct. 18, 1978

Owner: Noah Toews

Driller: Schmidt Drilling Est. rate of Production: 25-30 igpm

(Airlift)

	Drif	t	
0	-	5	Till, silt, brown, sandy and clayey, pebbles
5	-	10	Till, silt, brown, sandy and clayey, pebbles, some coal chips
10	-	20	Till, silt, greyish brown, sandy and more clayey, pebbles, some coal chips
25	-	40	Clay, brownish grey to grey silty and sandy with some pebbles and coal chips
40	-	90	Sandy silty clay, grey with plenty of sand medium to course grain, pebbles and coal chips
90	-	100	Sandstone (as a piece of bedrock greenish grey, very fine grain, hard)
100	-	105	Coarse sand
105	-	126	Gravel, very coarse gravel 1-3" size, loose, chert, quartz felds with coal chips
Bedrock		ck	
126	-	128	Sandstone - Bedrock: light grey, fine to medium grain argillaceous bentonitic
		128	Bottom of Hole
			· · · · · · · · · · · · · · · · · · ·
		-	Hole E-logged
		-	Reamed the hole from 4 1/2" to 6 3/4"
		-	Drilling mud additive "magcogel" used during the drilling
		- *	126 ft of 5 $1/2^{\text{H}}$ casing installed (12 ft slotted casing at the bottom included)
		-	Drilling started at 10:30, finished at 15:30
			Airlift production rate 25-30 igpm
¥8		-	Measured depth of well = $125.60 \text{ ft } (38.28 \text{m})$
		-	Water sample taken for chemical analyses

NEW NORWAY SEISMIC PROJECT EXPLORATION SITE 3 PILOT WELL #3 DN (Drift North)

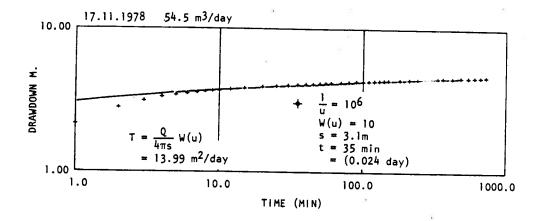
Water Level Measurements

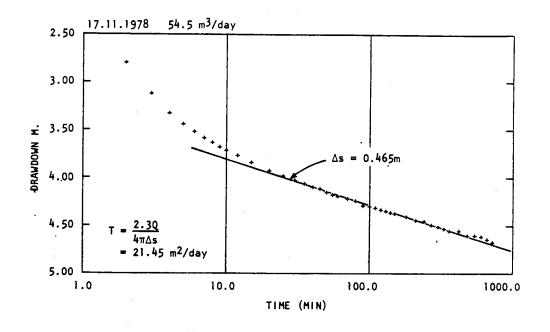
Date		Time	Water Level	<u>(m)</u>
Oct.	18/78	3.55	9.63	
Oct.	19/78	8.35	6.41	
Oct.	19/78	9.35	6.23	
Oct.	19/78	10.35	6.08	
Oct.	19/78	11.40	6.08	
Oct.	19/78	13.50	5.62	
Oct.	19/78	14.50	5.65	
Oct.	19/78	16.05	5.63	
Oct.	20/78	8.30	5.74	
Oct.	23/78	9.20	5.63	
Oct.	24/78	11.15	5.58	

Appendix B

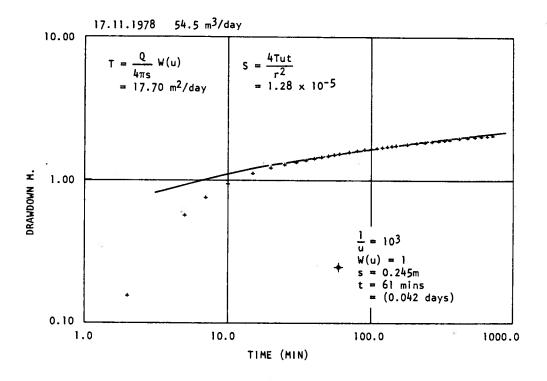
PRE-DETONATION AQUIFER AND WELL PERFORMANCE TESTS

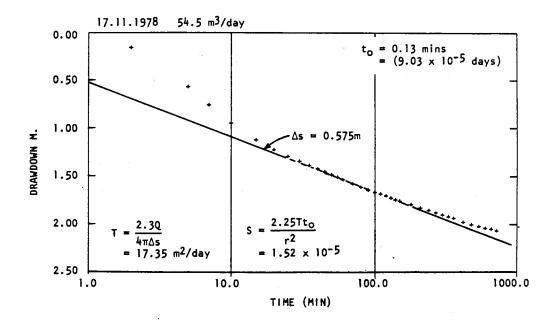
DSAT 1
PUMPING WELL



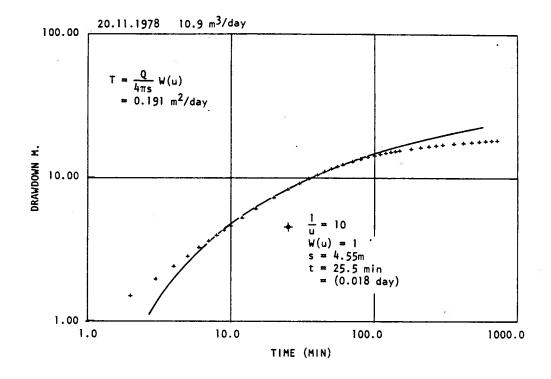


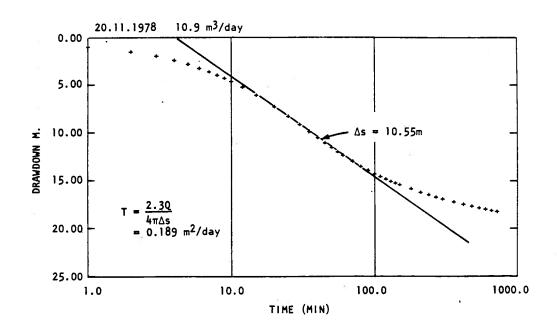
DSAT 1 OBSERVATION WELL R = 15.239 m



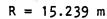


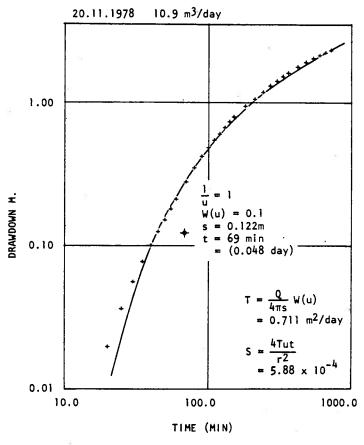
BOHAT 1 PUMPING WELL

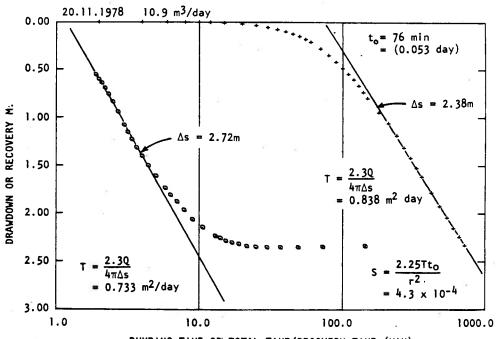




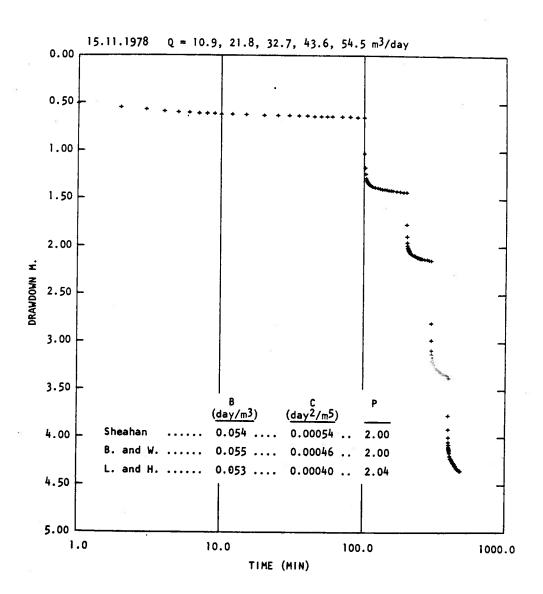
BOHAT 1 **OBSERVATION WELL**

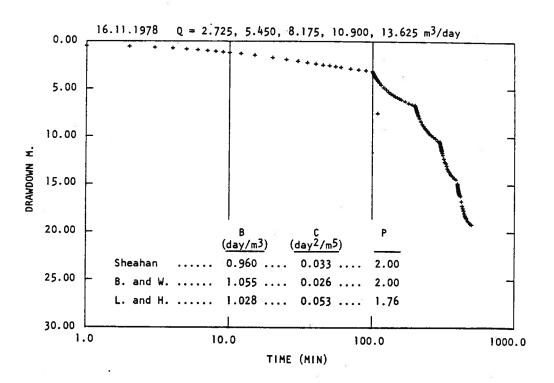


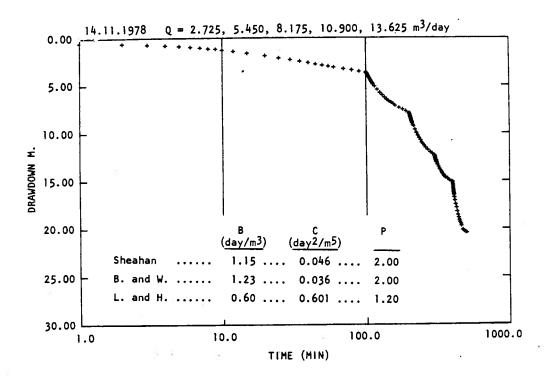




PUMPING TIME OR TOTAL TIME/RECOVERY TIME (MIN)



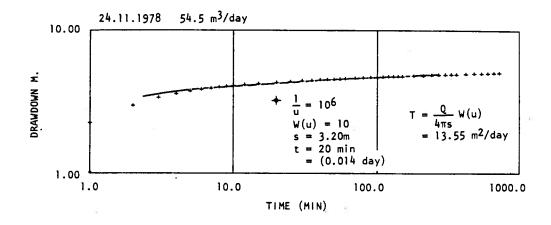


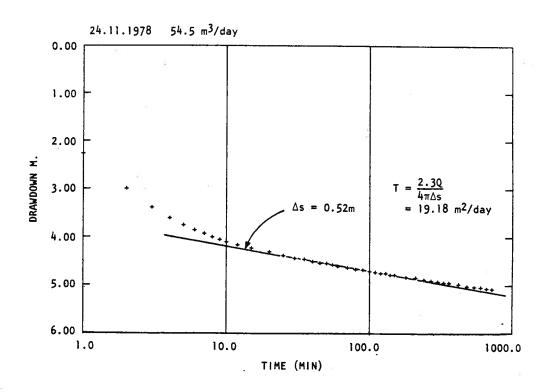


Appendix C

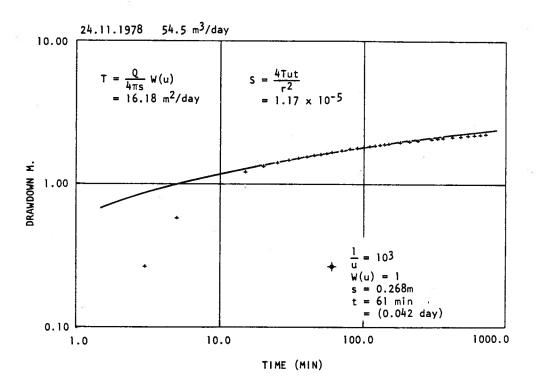
POST-DETONATION AQUIFER AND WELL PERFORMANCE TESTS

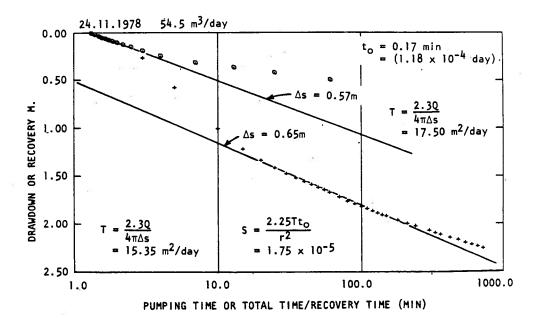
DSAT 2 PUMPING WELL



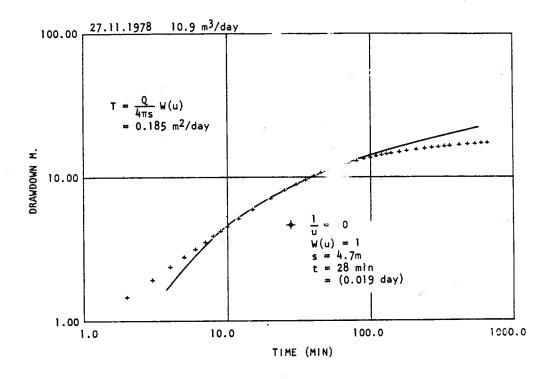


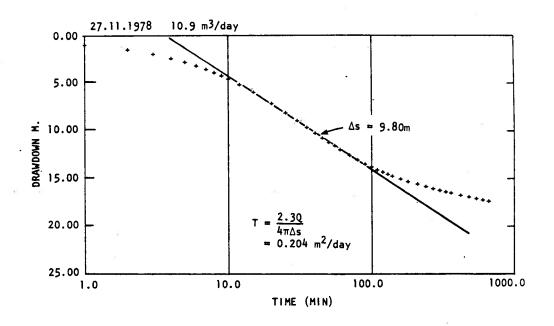
DSAT 2 OBSERVATION WELL R = 15.239 m



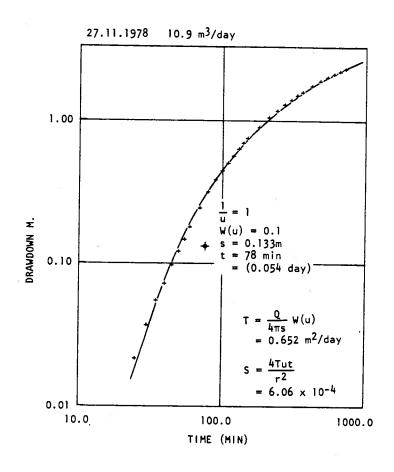


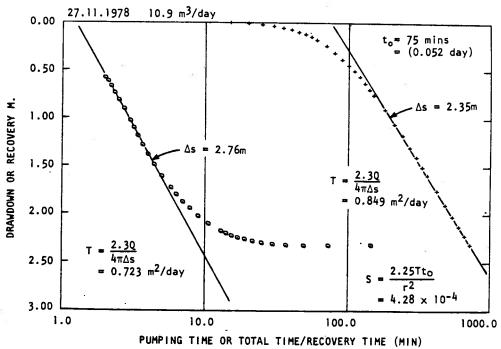
BOHAT 2 PUMPING WELL



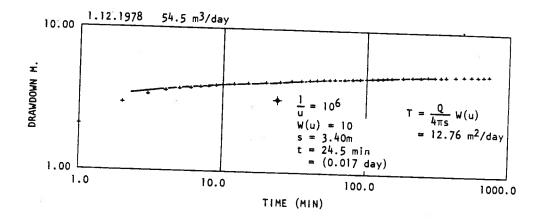


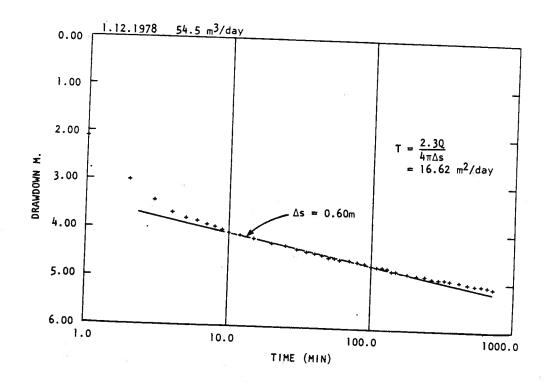
BOHAT 2 OBSERVATION WELL



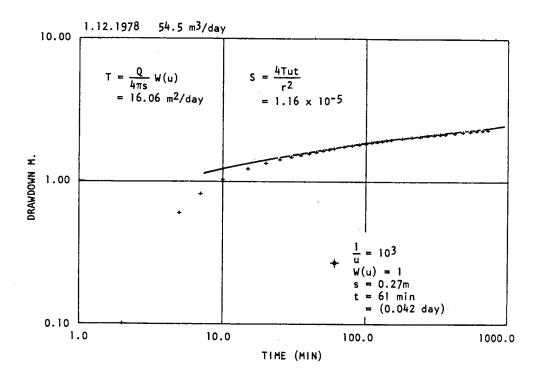


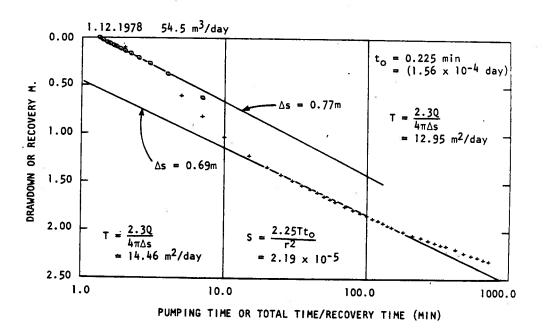
DSAT 3 PUMPING WELL



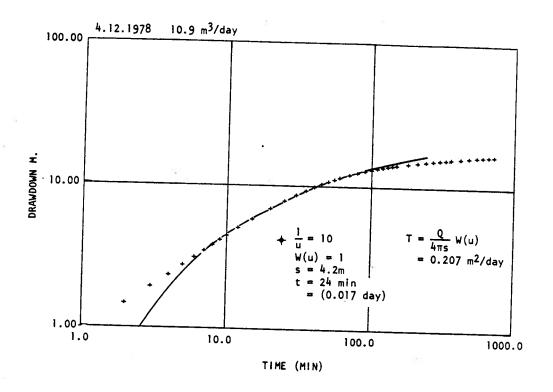


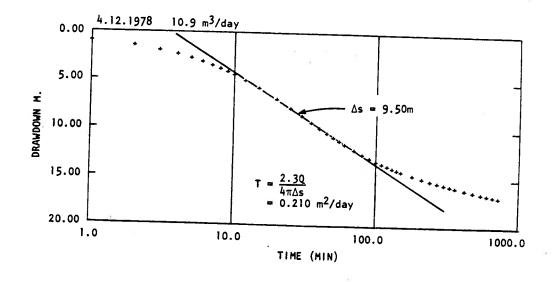
DSAT 3 OBSERVATION WELL R = 15.239 m



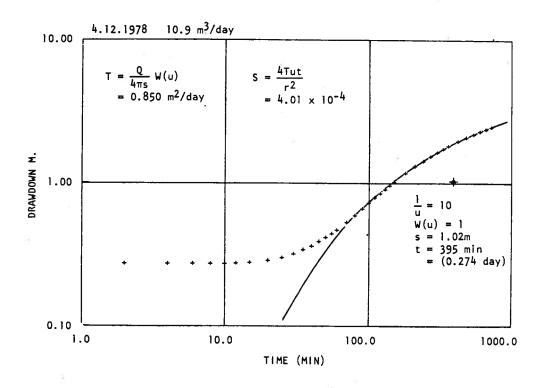


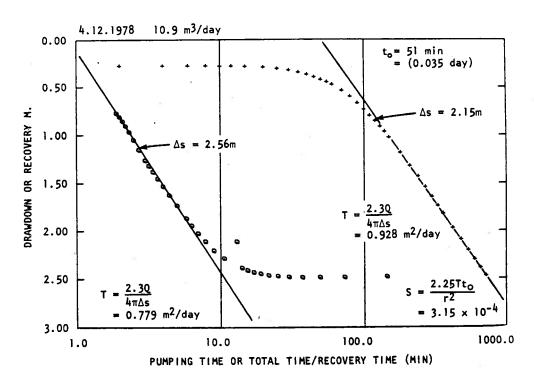
BOHAT 3 PUMPING WELL



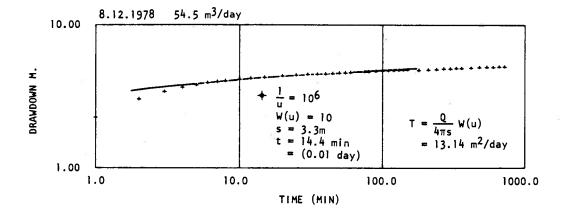


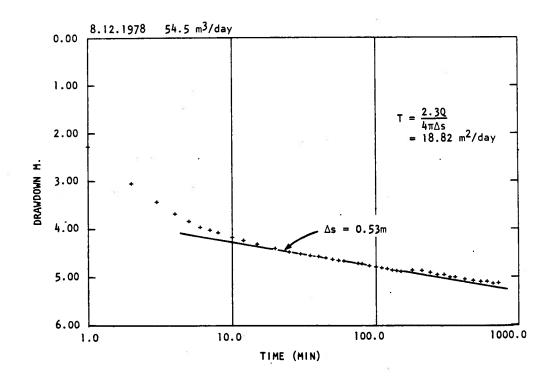
BOHAT 3 OBSERVATION WELL R = 15.239 m



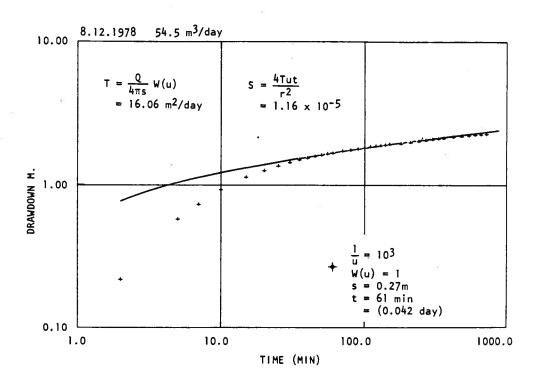


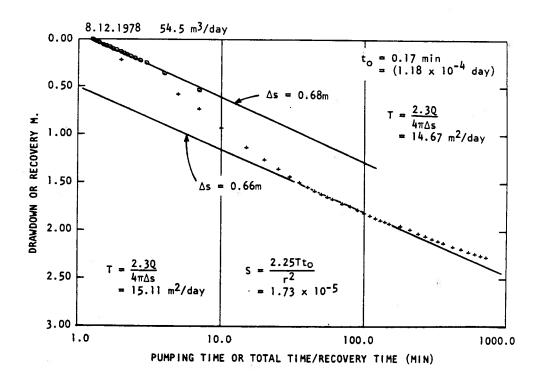
DSAT 4
PUMPING WELL



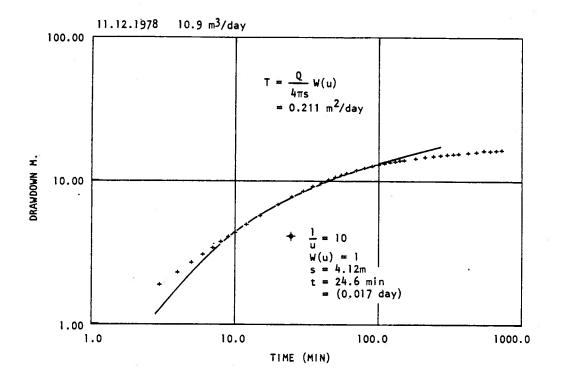


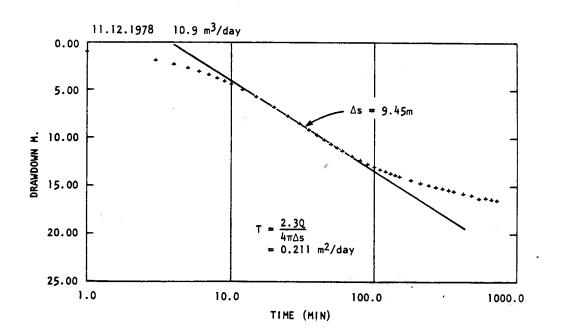
DSAT 4
OBSERVATION WELL



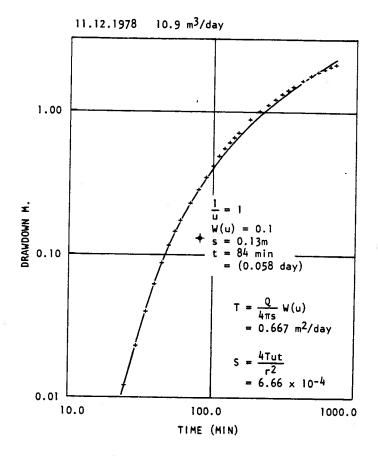


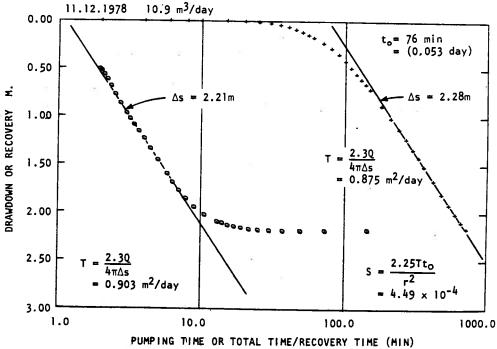
BOHAT 4 PUMPING WELL



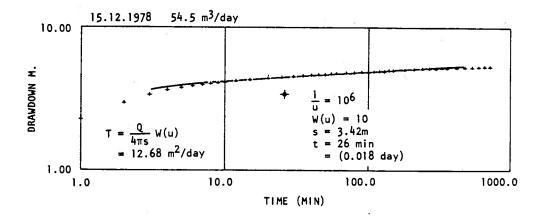


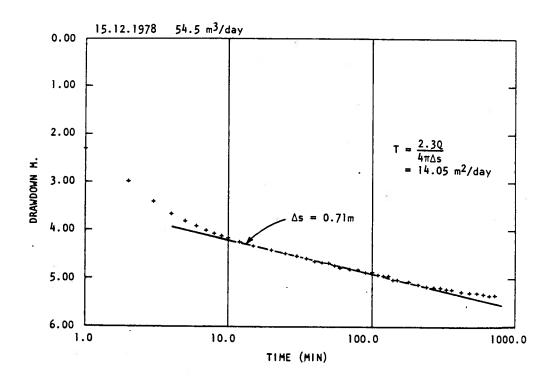
BOHAT 4 OBSERVATION WELL R = 15.239 m



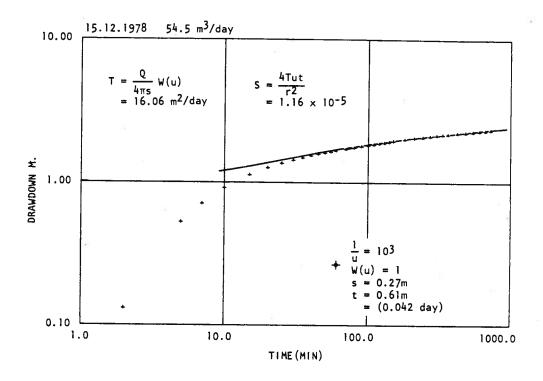


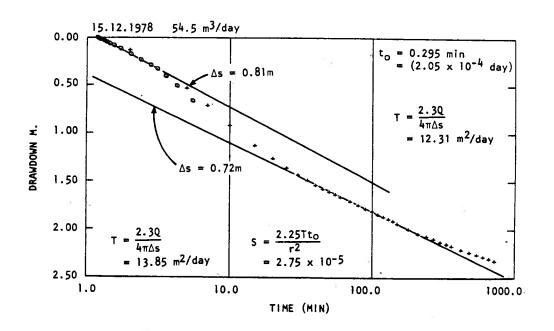
DSAT 5 PUMPING WELL



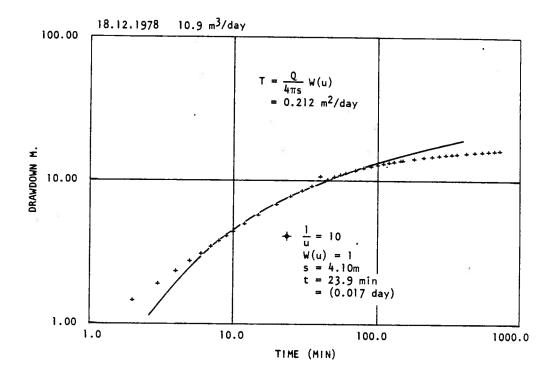


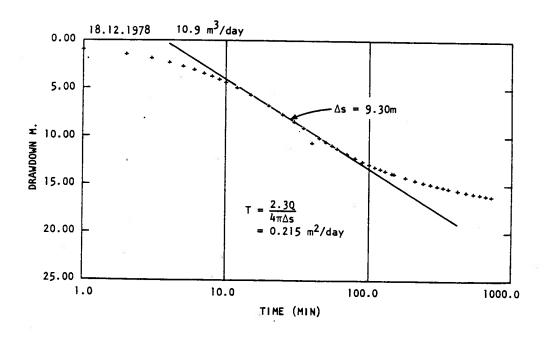
DSAT 5 OBSERVATION WELL R = 15.239 m





BOHAT 5 PUMPING WELL

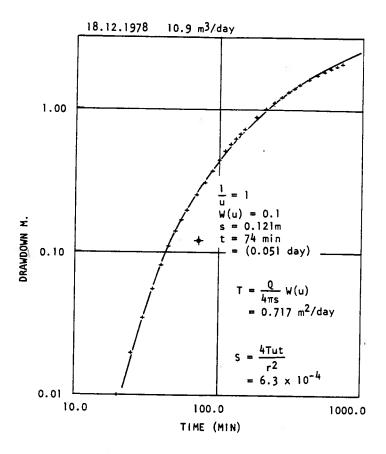


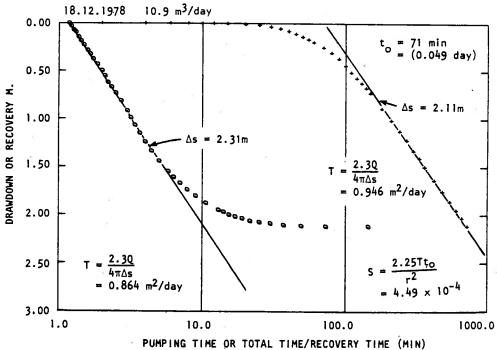


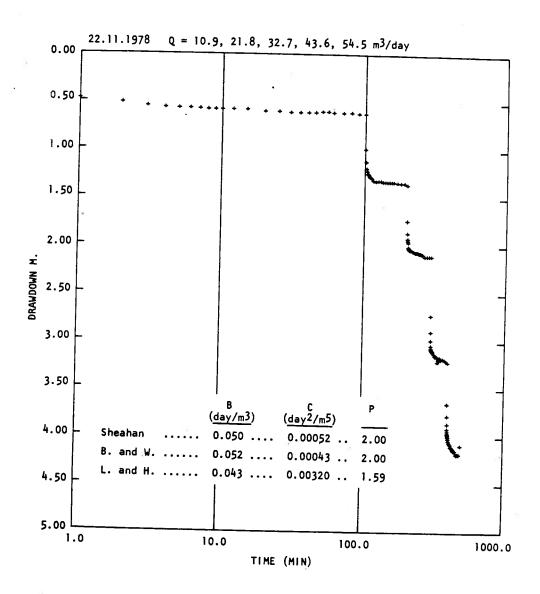
BOHAT 5

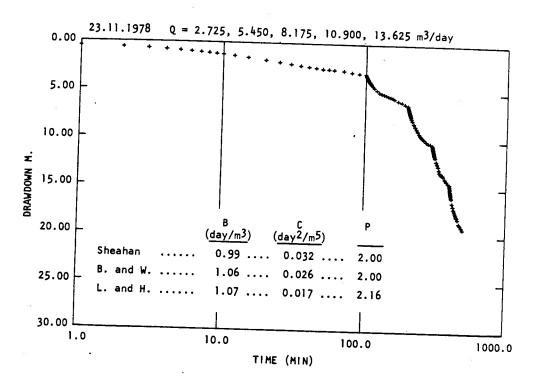
OBSERVATION WELL

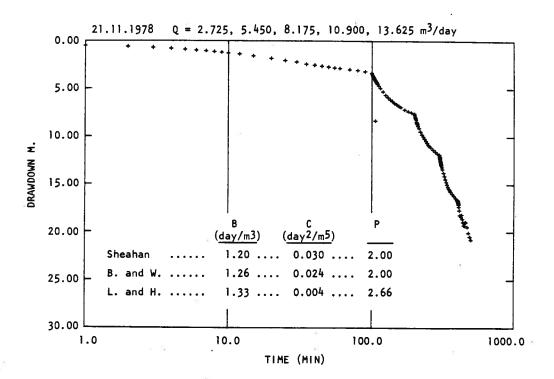
R = 15.239 m

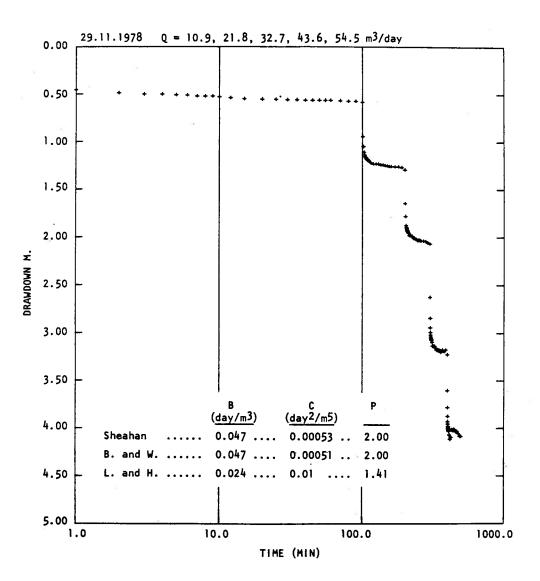


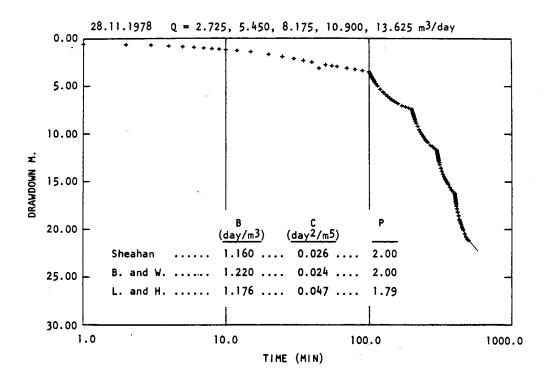


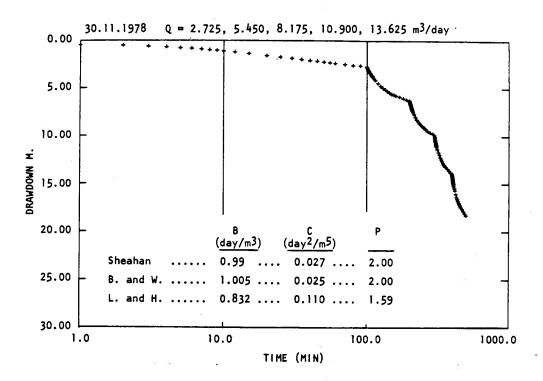


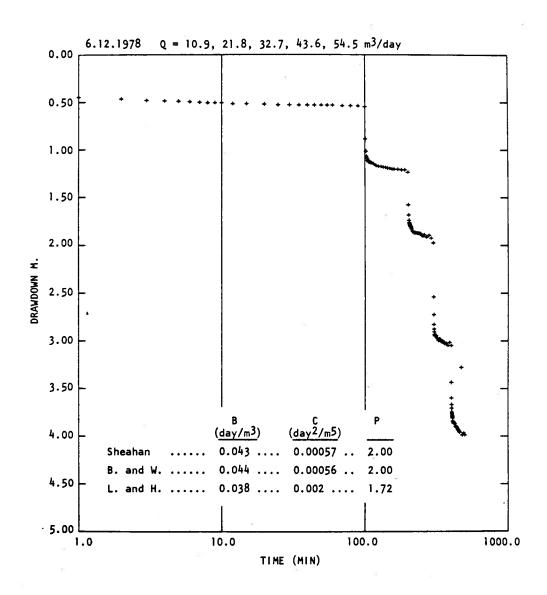


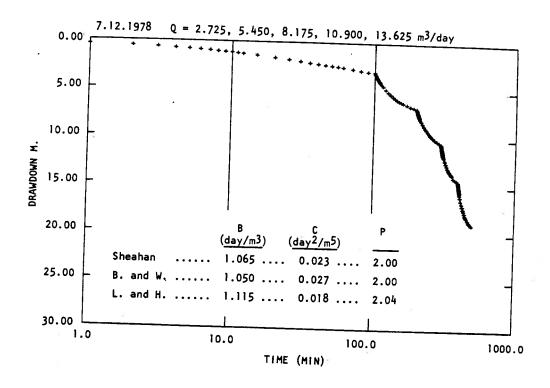


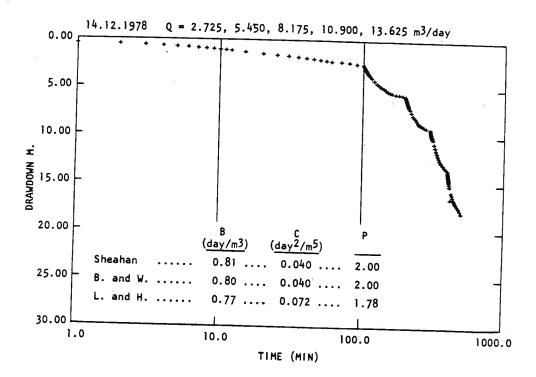


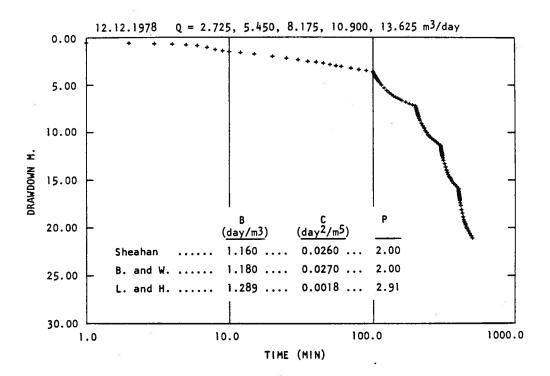












Appendix D

HYDROCHEMICAL DATA - SUMMARIES AND ANALYSES

					1	SAT				
	DSA	T-1	DSA	NT-2	DSA	AT-3	DSA	\T-4	DSA	T-5
	30 Mins	End ppm	30 Mins ppm	End ppm	30 Mins	End ppm	30 Mins	End ppm	30 Mins	End ppm
TDS	1732	1738	1662	1694	1758	1826	1046	1636	1628	1646
Alk.	504.0	515.2	443.2	-17.6	544.8	566.4	562.4	520.8	454.4	509.6
ard.	846.7	836.8	807.6	794.0	888.4	916.5	939.0	899.1	838.3	885.7
рН	7.6	7.8	7.7	7.8	7.8	7.6	7.4	7.6	7.6	7.5
Na	179.0	178.0	184.0	183.0	184.0	185.0	190.0	189.0	186.0	186.0
K.	7.1	6.7	7.9	7.1	7.9	7.9	6.7	6.7	5.4	5.4
Ca	214.0	215.0	200.0	193.0	234.0	242.0	251.0	235.0	209.0	228.0
Mg	76.0	73.0	75.0	76.0	74.0	76.0	76.0	76.0	77.0	77.0
C1	4.0	6.0	4.0	2.0	20.0	4.0	4.0	4.0	4.0	4.0
so ₄	643.0	600.0	688.0	687.0	698.0	679.0	723.0	673.0	758.0	742.0
NO ₃	1.5	0.2	1.6	0.0	0.8	0.0	0.3	0.1	2.8	0.0
⁰ 3	630.0	644.0	554.0	522.0	681.0	708.0	703.0	651.0	568.0	637.0

•

						SWT			19	
	DSV	√T-1	DSW	/T-2	DSW	л-3	DSW	IT-4	. DSW	/T-5
	30 Mins	End ppm								
TDS	1560	1604	1800	1792	1682	1598	1720	1602	1598	1726
Alk.	332.0	396.0	566.4	550.4	394.4	340.0	544.8	468.8	513.6	569.6
ard.	766.7	823.2	901.6	880.0	801.6	745.9	875.3	798.7	883.4	952.2
рΗ	7.5	7.6	7.6	7.5	7.9	7.7	7.8	7.8	7.8	7.5
Na	174.0	179.0	178.0	179.0	184.0	185.0	188.0	188.0	188.0	188.0
<u></u>	6.7	7.5	7.5	7.5	7.1	7.1	6.7	6.3	6.7	5.8
a	177.0	198.0	236.0	229.0	191.0	167.0	237.0	203.0	232.0	253.0
lg	79.0	80.0	76.0	75.0	79.0	80.0	69.0	71.0	74.0	78.0
:1	4.0	4.0	6.0	4.0	2.0	2.0	6.0	8.0	4.0	4.0
504	668.0	692.0	61.3.0	699.0	778.0	778.0	748.0	778.0	728.0	743.0
103	4.5	2.8	0.0	3.0	0.3	2.6	0.1	0.3	0.2	0.3
10 ₃	415.0	495.0	708.0	688.0	493.0	425.0	.681.0	586.0	642.0	712.0

= 20

					BS	CWT				-
	BSCW	T-1	BSCW	T-2	BSCW	T-3	BSCW	T-4	BSCW	T-5
	30 Mins	End ppm								
TDS	1456	1394	1474	1348	1586	1308	1704	1282	1474	1262
Alk.	587.2	611.2	616.8	599.2	572.0	528.8	584.0	482.0	628.8	624.8
Hard.	134.9	289.1	203.4	317.3	251.5	229.3	218.0	175.2	228.0	313.2
pН	8.1	7.7	7.0	7.2	7.2	7.8	7.6	8.5	7.7	7.5
Na	470.0	365.0	475.0	365.0	453.0	371.0	476.0	381.0	465.0	390.0
К	2.5	2.9	2.9	2.9	1.7	2.1	4.2	3.3	2.9	2.5
Ca	30.0	73.0	53.0	81.0	66.0	49.0	61.0	29.0	65.0	81.0
Mg	14.6	26.0	17.3	28.0	21.1	26.0	16.0	25.0	16.0	27.0
C1	10.0	10.0	4.0	8.0	8.0	8.0	10.0	10.0	14.0	10.0
so ₄	448.0	391.0	520.0	428.0	512.0	502.0	564.0	450.0	563.0	437.0
NO ₃	1.8	2.0	0.0	2.5	0.0	0.1	0.1	0.0	0.1	0.1
HCO 3 CO 3	734.0	764.0	771.0	749.0	715.0	661.0	730.0	587.4	786.0	781.0

					B	онwт				
_	вонw	T-1	воны	/T-2	воны	/T-3	воны	T-4	вонw	T-5
	30 Mins	End ppm								
TDS	1512	1302	1234	1242	1422	1262	1338	1258	1260	120
Alk.	636.0	607.2	630.4	507.9	615.2	630.4	601.6	628.8	634.4	628.8
Hard.	80.9	203.7	136.7	144.7	187.3	256.1	170.3	277.7	193.1	269.0
рН	7.8	7.9	7.8	8.4	8.1	8.1	7.4	7.7	7.6	7.:
Na	520.0	379.0	430.0	381.0	436.0	381.0	439.0	385.0	429.0	379.0
К	2.5	2.9	1.7	3.3	3.8	2.9	1.7	2.9	1.7	2.5
Ca	24.0	49.0	36.0	25.0	49.0	68.0	45.0	75.0	51.0	60.0
Mg	5.1	19.8	11.4	20.0	15.8	21.0	14.1	22.0	16.0	29.0
C1	14.0	14.0	36.0	6.0	20.0	16.0	22.0	14.0	24.0	14.0
so ₄	500.0	311.0	383.0	383.0	398.0	334.0	375.0	348.0	368.0	362.0
NO ₃	0.0	2.4	0.1	1.4	0.0	0.0	0.2	0.2	0.3	0.0
HCO3	795.0	759.0	788.0	622.0	769.0	788.0	752.0	786.0	793.0	786.0

•

					во	TAH	,	,		
	ВОНА	T-1	вона	T-2	вона	T-3	вона	T-4	ВОНА	т-5
	30 Mins	End ppm								
TDS	1414	1256	1472	1181.3	1370	1270	1378	1212	1258	1258
Alk.	634.4	626.4	638.4	558.4	566.3	628.8	636.0	634.4	634.4	626.4
Hard.	157.9	226.6	228.7	161.3	139.4	233.8	229.6	247.0	250.2	262.6
рН	7.9	7.9	8.1	8.3	8.4	7.8	7.7	7.7	7.8	8.0
Na	443.0	373.0	454.0	384.0	454.0	384.0	449.0	390.0	443.0	384.0
ĸ	2.5	2.9	2.9	2.5	2.5	4.2	2.5	2.1	2.1	1.3
Ca	42.0	56.0	60.0	30.0	29.0	64.0	64.0	66.0	64.0	64.0
Mg	12.9	21.1	19.2	21.0	16.3	18.0	17.0	20.0	22.0	25.0
C I	18.0	18.0	12.0	12.0	12.0	20.0	14.0	16.0	14.0	4.0
so ₄	408.0	322.0	469.0	379.0	463.0	360.0	464.0	331.0	484.0	339.0
NO ₄	0.5	0.0	0.0	0.0	0.0	0.4	0.2	0.2	0.0	0.0
1¢03 co3	793.0	783.0	798.0	698.0	695.0	786.0	795.0	793.0	793.0	783.0

Mer	4 1	p 45	Rge	22	Sec	14	Lsd	11			
Lab no. Index no. Well depth(f Water level(Top open int Bottom open Altitude(ft) Bedrock elev TDS(mg/l) Field Cond(m Field pH	ft) erval(f interva ation(f	1(ft) t)	1738.0		Date Date Date Sampl Sampl Owner Hardr	analy led by le Sours nam less(a linity	itted ysed(n ysed(n yrce ne ss CaC	najor) ninor) 203) 2aCO3) /cm#25	20 3 R VC 7 NE	11 11 10 10 10 10 10 10 10 10 10 10 10 1	78 79 LL IIN ED

MAJOR CONSTITUENTS

	<u> </u>	*	of total anion
.	mg/1	meq/1	or cation
Calcium(Ca)	215.0	10.73	43.5
Magnesium(Mg)	73.0	6.01	24.4
Sodium(Na)	178.0	7.74	
Potassium(K)			31.4
	6.7	0.17	0.7
Carbonate(CO3)	Ø • Ø	0.00	0.0
Bicarbonate(HCD3)	644.0	10.50	45.5
Sulphate(SO4)	600.0	12.49	*
Chloride(Cl)	6.0	Ø.17	53.8
Nitrate(NO3)	-		9.7
Hydroxide (OH)	0.2	0.00	∌.0
\$111ca(\$102)	9.8	Total anions(epm)	23,220
Calcium(Acid)	235.0	Total cations(epm)	- 100
Magnestum (Acid)	75.0		24.651
	· •	Ion balance error(%)	
Calculated TDS	1405.4	TDS balance error(%)	-19 .

MINOR CONSTITUENTS 7.6 ppm

Iron

OTHER MEASUREMENTS 5.50 Fluoride(F)

Field Temp(C)

0.10 ppm

Mar 4	Tp	45	Rge	22	Seç	14	Led	11			
			100						D	M	Y
Leb no.			1054		Date	Samp	e d		24	11	78
Index no.		48	4522		Date	submi	tted			12	
Well depth(ft)			83.0					(noles	5		79
Water level(ft) =		28.5					inor)	•	•	/ >
Top open inter	val(ft)		72.0			ed by		HOP	R V)GW)	111
Bottom open in	tervel(ft)	83.0			e Sou				DS	
Altitude(ft) Bedrock elevat					Owner	. nem	•		;	1 DE	11N
TOOK	100(15)					1088(8				807	. 6
TDS(mg/1)		16	62.0		Alkal	inity	(48 (aC03)		443	
Field Cond(mic	romh@#/	ÇM)						cm#251	C 3		350
Field pH					Lab p				- •		7

MAJOR CONSTITUENTS

		X (of total anion
	mg/1	meq/1	or cat on
Calcium(Ca)	200.0	9,98	41.0
Magnesium(Mg)	75.0	6,17	25.3
Sodium (Na)	184,0	8.00	
Potassium(K)	7.9		32.9
		0.20	. Ø,8
Carbonate(CO3)	0.0	0.00	0.0
Bicarbonate(HCQ3)	554.0	9.08	38.6
Sulphate(\$04)	688.0	14.32	60.8
Chloride(C1)	4.0	0.11	0,5
Nitrete(NO3)	1.6	•	
Hydroxide(OH)	1.0	0.03	0.1
	_		
8111ça(8102)	14.7	Total anions(epm)	23.543
Calctum(Actd)	230.0	Total cations(epm)	24.358
Magnesium (Açid)	73.0	Ion balance error(%)	• •
Calculated TDS	1447.6		
	4-7/00	TDS balance error(%)	•13 ,

MINOR CONSTITUENTS

Iron

8,6 ppm

OTHER MEASUREMENTS 6.50 Fluoride(F)

Mer 4 Tp 4	5 Rge	22	Sec	14	Lsd	11			
Lab no. Index no. Well depth(ft) Water level(ft) Top open interval(ft) Bottom open interval(ft Altitude(ft) Bedrock elevation(ft) IDS(mg/l) Field Cond(micromhos/cm	781055 404522 83.0 28.5 72.0 82.0	22	Date Date Date Sampl Sampl Owner Hardn	samo! submi analy analy led by le Sou is nam less(a	ed tted sed(n rce e s CaC	major) minor)	01 5 R V	11 12 1 0GV: 0SV: 792 417	78 79 ILL AT2 END
Field pH			Lab p			VIII V E V I	, s		7 . 8

MAJOR CONSTITUENTS

		% o	f total anion
	mg/1	mea/1	or cation
Calcium(Ca)	193.0	9.63	40.1
Magnestum(Mg)	76.0	6.26	26.0
Sodjum (Na)	183.0	7.96	33.1
Potassium(K)	7.1	0.18	0.8
Carbonate(CO3)	0.0	0.00	Ø . 0
Bicarbonate(HCO3)	522.0	8.56	37.3
Sulphate(SO4)	687.0	14.30	62.4
Chloride(Cl)	2.0	Ø . Ø 6	0.2
Nitrate(NO3)	0.0	0.00	0.0
dydroxfde(OH)		- •	***
Silica(SiO2)	14,6	Total anions(epm)	22,916
Calcium(Acid)	231.0	Total cations(epm)	24.027
Magnestum(Actd)	68.0	Ion balance error(%)	2.
Calculated TDS	1419.4	TDS balance error(%)	-16.

MINOR CONSTITUENTS

Iron 5.6 ppm

OTHER MEASUREMENTS Fluoride(F)

0.00 ppm

	Men	4	Tp	45	Rge	22	Sec	14	Lad	11			
				52							D	M	Y
tab no.				78	1060		Dete	Samp	led		1	12	78
Index no	•			40	4522			submi				12	
Well dep	th(†	t)			84.0					melor)	5		79
Water le	vel(ft)			30.0					ninor)		•	, ,
Top open	int		1(ft)		72.0			ed by		⊚	٧٢)GW	r
Bottom o	pen	inte	rval(82.0			e So			•	08	
Altitude		,		. • •	- - -		-	** na:			30	3 M 3	
Bedrock		atio	n(ft)					1088(4	-	033	76	888	
TDS(mg/1		,-		17	58.0					CeC03)			-
Field Co	nd (m	cno	mhos/	rm)					0.6	/cm#25C)		544	-
Field pH		1 2 1.0	··· 11 🗸 🗸 7 1	# III /				-	3 m Li O 2 /	CWASOC1			900
1 14 10 pi							Leb p	חק				/	7. 8

MAJOR CONSTITUENTS

		* 0	f total anion
	mg/1	meq/1	or cation
Calctum(Ca)	234.0	11.68	45.8
Magnestum(Mg)	74.0	6.09	23.4
Sodium (Na)	184.0	8.00	30.8
Potassium(K)	7.9	0.20	0,8
Carbonate(CD3)	0.0	0.00	0.0
Bicarbonate(HCO3)	681.0	11.16	42.5
Sulphate(SO4)	698.0	14.53	55.3
Chloride(Cl)	20.0	0.56	2,1
Nitrate (NO3)	0.8	0.01	0.0
Hydroxide(OH)		·	
\$111ça(8102)	14.5	Total enions(epm)	26,272
Calcium(Agid)	245.0	Total cations(epm)	25.973
Magnesium(Açid)	75.0	Ion balance error(%)	1.
Calculated TDS	1568.0	TDS balance error(%)	-11,

MINOR CONSTITUENTS

Iron

7.6 ppm

OTHER MEASUREMENTS 5.90 Fluoride(F)

Men 4 Tp	45 Rge	22 Sec 14 Lad 11	
Leb no. Index no. Well depth(ft)	781061 404522 84.0	Date sampled Date submitted	D M Y 1 12 78 8 12 78
Water level(ft) Top open interval(ft) Bottom open interval(30.0 72.0	Date analysed(minor) Sampled by	5 1 79 Vogwill
Altitude(ft) Bedrock elevation(ft) TDS(mg/1)	ft) 82.0 1826.0	Sample Source Owners name Hardness(as CaCO3)	DSAT3 END 916.5
Field Cond(micromhos/ Field pH	ČW) 1950∮A	Alkalinity(as CaCO3) Cond(migromhos/gme25C) Lab pH	566.4 1000 7.6

MAJOR CONSTITUENTS

		X G	if total anion
	mg/1	meq/1	or cation
Calcium(Ca)	242.0	12.08	45.4
Magnestum(Mg)	76.0	6.26	23.5
Sodium(Na)	185.0	8.05	30.3
Potassium(K)	7.9	0.20	
Carbonate(CO3)	9.0	0.00	0,8
Bicarbonate (HCO3)	708.0		0.0
Sulphate (804)	•	11.60	44.9
	679.0	14.14	54 . 7
Chloride(C1)	4.0	0.11	0.4
Nitrate(NO3)	0.0	0.00	0.0
Hydroxide(OH)		•	
8111ca(8102)	14.5	Total anions(epm)	25.854
Caistum (Asid)	235.0	Total cations(epm)	26.580
Magnesium(Acid)	72.0	Ion balance error(%)	
Calculated TDS	1556.5	The belonce accords	1.
		TDS balance error(%)	-15.

MINOR CONSTITUENTS

Iron

5.6 ppm

Field Temp(C)

OTHER MEASUREMENTS 5.90 Fluoride(F)

0.1

meja bbw

Mer	4 Tp	45 Rge	22	Sec 1	14	Lad	11			
								D	M	Y
Lab no.		781070		Date s	ample	d			12	
Index no.		464522		Date s					12	-
Well depth(ft)	83.4		Date a				-	1	-
Mater level(f	t)	30.0		Date a					•	
Top open inte	rval(ft)	72.0		Sample				V) GW I	[1]
Bottom open i	nterval (1	(t) 82.0		Sample				•	DS	-
Altitude(ft)				Owners				:	30M]	
Bedrock eleva	tion(ft)			Hardne			03)	•	939	
TDS(mg/1)		1046.0					aC03) ·		562	-
Field Cond(mi							cm@250)			170
Field pH	2			Lab pH			Ç & 2.00)			4

MAJOR . CONSTITUENTS

				of total anion
	mg/1		meq/1	or cation
Calcjum(Ca)	251,0		12.52	46.0
Magnestym(Mg)	76.0		6.26	23.0
Sodium (Na)	190.0		8.26	30.4
Potassium(K)	6 . 7		0.17	0.6
Carbonate(CO3)	0.0		0.00	0.0
Bicarbonate(HCO3)	703.0		11.52	43,2
Sulphate(SO4)	723.0		15.05	56.4
Chloride(C1)	4.0		0.11	0.4
Nitrate(NO3)	0.3		0.00	0.0
Hydroxide(OH)			·	• •
Silica(SiO2)	15.1	(90)	Total anions(epm)	26.693
Calcium(Acid)	234.0		Total cations(epm)	27.216
Magnesium (Acid)	77.0		Ion balance error(%	
Calculated TDS	1611.8		TDS balance error(%	

MINOR CONSTITUENTS

Iron 10 ppm

OTHER MEASUREMENTS 6.00 Fluoride(F)

	Mer	4	Ţp	45	Rge	22	Sec	14	Lsd	11			
											D	М	Y
Lab no.				78	1071		Date	samo	led		8	12	
Index no				40	4522				itted			12	
Well dep					83.0					najor)	9		79
Water le					30.0					ninor)	-	•	, ,
Top open					72.0		Sampl				٧٢)Gw.)	T i i
Bottom of		inter	val(ft)	82.0		Sampl					DSA	
Altitude							Owner						ND
Bedrock									as Ca(203)		899	
TDS(mg/l)				36.0					(aCO3)		526	-
Field Co	nd(m	Cron	hos/	cm)						cm=25			12vi
Field pH							Lab p				065		7.6

MAJOR CONSTITUENTS

		X	of total anion
	mg/1	meq/1	or cation
Calcium(Ca)	235.0	11.73	44.5
Magnestum(Mg)	76.U	6.26	23.7
Sodfum(Na)	189.0	8,22	31.2
Potassium(K)	6.7	0.17	0.6
Corbonate(CO3)	0.0	0.00	0.0
bicarbonate(HCO3)	651.0	12.67	43.0
Sulphate(SO4)	673.0	14.01	56.5
Chloride(Cl)	4.0	0.11	0.5
Nitrate(NO3)	0.1	0.00	0.0
Hydroxide(OH)		~ ·	
Silica(SiD2)	17.0	Total anions(epm)	24.797
Calcium (Acid)	239.0	Total cations(epm)	
Magnesium(Acid)	73.0	Ion balance error(
Calculated TDS	1520.9	TDS balance error(

MINOR CONSTITUENTS

Iron

6.9 ppm

OTHER MEASUREMENTS 6.60 Fluoride(F)

Me	4	Tp.	45	Rge	22	Sec	14	Led	11			
										D	M	Y
iab no.				1091		Date	samp	led		15	12	•
Index noe			48	4522			submi				01	
Well depth(t)			83.0					nejor)	10		79
Water level	ft:)		28,5					ninor)		•	, ,
Top open int	•	val(fe)		72.0			ed by		"THOP'	R V	OGW;	7 1 1
Bottom open	in	tervel	řt)	82.0			e Sou				DSA'	
Altitude(ft)	1					•	'S nen					100000
Bedrock elev		1/4-1								•	30	-
The same of the	d f	10111167					1088(4				838	3.3
TD3(mg/)			16	28.0		Alkal	inity	/(as ((aCO3)		454	1.4
Field Cond(1101	romhos/	cm)						cm#251	2.3		40
Field pH			-						C III A IE O I			
- 1 - 1 - 1						Lab p	717				7	7.6

MAJOR CONSTITUENTS

		· * * * * * * * * * * * * * * * * * * *	total anion
• • • • •	. mg/1	meq/1	or cation
Calcium(Ca)	209.0	10.43	41.7
Magnestum (Mg)	77.0	6.34	25.4
Sodium(Na)	186.0	8.09	32.4
Potassium(K)	5.4	0.14	_
Carbonate(CO3)	0.0	<u> </u>	0,6
Bicarbonate (HCO3)		0.00	0.0
	568.0	9.31	36,9
Sulphate (804)	758.0	15,78	62,5
Chioride (Ci)	4.0	0.11	0,4
Nitrate(NO3)	2.8	0.05	0.2
Hydroxide(OH)	_ 🔻		w, c
8111ca(8102)	13,4	Total enions(epm)	25,250
Calcium(Acid)	245.0	Total cations(epm)	24,995
Magnestum(Agid)	78.0	Ion balance error(%)	
Calculated TDS	1534.9	TDS balance error(%)	1. -6.

MINOR CONSTITUENTS

Iron

12 ppm

OTHER MEASUREMENTS

6.88 Fluoride(F

Field Temp(C)

8.28 pps

Leb no. 781092 Index no. 404522 Well depth(ft) 83.0 Water level(ft) 28.5 Top open interval(ft) 72.0 Bottom open interval(ft) 82.0 Altitude(ft) Bedrock elevation(ft) Hardness(as CaCO3) Date sampled 15 12 7 Date submitted 64 01 7 Date enalysed(major) 10 1 7 Date enalysed(minor) Sampled by R VOGWILI Owners name ENI Hardness(as CaCO3)	Mer 4	Tp 45	Rge	2 2	Sec 1	4 L	.sd	11			
TDS(mg/) 1646.0 Alkalinity(as CaCO3) 509.0 Cond(migromhos/cm) Cond(migromhos/cme25C) 1990 Lab pH 7.5	Index no. Well depth(ft) Weter level(ft) Top open interval(Bottom open interval(Altitude(ft) Bedrock elevation(TDS(mg/) Field Cond(migromho	fe) el(ft) ft)	781092 404522 83.0 28.5 72.0 82.0		Date so Date and Date and Sample Sample Owners Hardnes Alkelin Cond(mi	ampled ubmitt nalyse nalyse d by Sourc name ss(as	i ed cod cod cod cod cod cod cod cod cod co	ojor) inor) 03) aCO3)	04 18 R V	12 01 1 0GW! 0SA1 885 509	79 79 ILL 5 ND 5.7

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(C1)	mg/1 228.0 77.0 186.0 5.4 0.0 637.0 742.0	meq/1 11.38 6.34 8.09 9.14 0.00 10.44 15.45	f total anion or cation 43.9 24.4 31.2 0.5 0.0 40.2 59.4 0.4
Nitrate(NO3) Hydroxide(OH) 8ilica(SiO2)	0,0	0.00	0.0
Calcium(Acid) Magnasium(Acid) Calculated TDS	14.8 225.0 68.0 1570.4	Total enjons(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	26.002 25.943 0. -5.

MINOR CONSTITUENTS

Iron

7.1 ppm

OTHER MEASUREMENTS 5.60 Fluoride(F)

8.18 ppm

Field Temp(C)

	Men	4	Tp	45	Rge	22	Sec	14	Lsd	11			
Lab no. Index no. Well deporter les Top open Bottom of Altitude Bedrock of TDS(mg/l) Field Cor	th(from the control of the control o	ft) Prval Inter Ition	va1 († (†e)	D8 't)	83.0 28.5 72.0 82.0		Date Dete Sampi Sampi Owner Herdn Alkei	subm enal enal e So s na ess(init	itted ysed(m ysed(m ysed(m y	inor) 03) 003)	20 3 R V(GW] PIL WST 636 189	78 79 LL .OT ED

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(Cl) Nitrate(NO3) Hydroxide(OH)	mg/1 123.0 80.0 184.0 8.3 0.0 237.0 752.0 6.0 3.5	meq/1 6.14 6.58 8.00 0.21 0.00 3.88 15.66 0.17 0.06	f total anion or cation 29.3 31.4 38.2 1.0 0.0 19.7 79.2 0.9 0.3
Silica(SiO2) Celcium(Acid) Magnesium(Acid) Celculated TDS	6.5 301.0 105.0 1279.8	Total enions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	19.767 20.938 3. -10.

MINOR CONSTITUENTS

Iron

38 ppm

OTHER MEASUREMENTS Fluoride(F)

0.00 ppm

Mer 4	Tp: 4	5 Rge	22	Sec 14 Led 11		
Lab no. Index no. Well depth(it) Water level(ft) Top open interval(Bottom open interval Altitude(ft) Bedrock elevation(it) TDS(mg/l) Field Cond(micromhorield ph	•1 († t f t)	1560.0		Date submitted Date enelysed(major) Date enelysed(minor)	15 1 20 1 3 VOG 30 NEW:	M Y 1 78 1 78 1 79 WILL MID 66.7 32.0 1860 7.5

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(C1) Nitrate(NO3)	mg/l 177.0 79.0 174.0 6.7 0.0 415.0 668.0 4.0	meq/1 8.83 6.50 7.57 0.17 0.00 6.80 13.91 0.11	of total anion or cation 38.3 28.2 32.8 0.7 0.0 32.6 66.6 0.5
Hydroxide(OH)	4.5	0,07	0,3
Siliga(SiO2) Calcium(Acid) Magnesium(Acid)	9.9 255.0	Total enions(epm) Total cations(epm)	20.896 23.074
Calculated TDS	74.0 1327.2	Ion balance error(%) TDS balance error(%)	5. ~15.

MINOR CONSTITUENTS

Iron 17.7 s

OTHER MEASUREMENTS 8,50 Fluoride(F)

Field Temp(C)

0.10 ppm

	Mer	4	Īp	45	Rge	22	Sec	14	Lsa	1 1			
Lab no. Index no Well dep Water le Top open Bottom op Altitude Bedrock e TDS(mg/1) Field Cor Field pH	th(fivel(finterpen in finterpen in fit) eleval)	ft) erval Inter	val(1 (ft)	DS(1027 WT 1 83.0 28.5 72.0 32.0		Date Date Date Samp! Samp! Owner Hardn	analy analy led by le Source s namess(a inity micro	itted /sed(m; /sed(m; / /rce	jor) inor) (3) (03)	20 3 R V E NE	11 11 15 500M EWST 823 396	78 79 ILL 11N ED
				MAJO	R ÇON	STIT	UENTS						
				_	-/1					% 01	tot	a l	anio

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(C1) Nitrate(NO3) Hydroxide(OH)	mg/1 198.0 80.0 179.0 7.5 0.0 495.0 692.0 4.0 2.8	mea/1 9.88 6.58 7.79 0.19 0.00 8,11 14.41 0.11	of total anion or cation 40.4 26.9 31.9 0.8 0.0 35.8 63.5 0.5 0.2
Silica(SiO2) Calcium(Acid) Magnesium(Acid) Colculated TDS	9.9 227.0 74.0 1416.6	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	22.679 24.442 4. #12,

MINOR CONSTITUENTS

Iron

8.1 ppm

OTHER MEASUREMENTS 6.50 Fluoride(F) ==

Megr	4	Tp.	45	Rge	22	Sec 14 Led 11			
Leb no. Index no. Well depth(f Hater level(Top open int Bottom open Altitude(ft) Bedrock elev TDS(mg/!) Field Cond(m Field pH	ft) erval inter ation	ve] (i (fe)	- 40 ft)	1032 4522 83.0 30.0		Date sampled Date submitted Date analysed(major) Date analysed(minor) Sampled by Sample Source Owners name Hardness(as CaCO3) Alkalinity(as CaCO3) Cond(migromhos/cme25)	27 3 .V0	11 11 1 0GW1 0SW1 901 566	78 79 ILL IT2 NS

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chioride(C1) Nitrate(NO3) Hydroxide(OH)	mg/1 236.0 76.0 178.0 7.5 0.0 708.0 613.0 6.0	meq/! 11.78 6.26 7.74 0.19 0.00 11.60 12.76 0.17 0.00	f total anion or cation 45.4 24.1 29.8 0.7 0.0 47.3 52.0 0.7 0.0
Silica(SiO2) Calcium(Acid) Magnesium(Acid) Calculated TDS	10.2 227.0 72.0 1474.8	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	24.537 25.966 3.

MINOR CONSTITUENTS

Iron

11,4 ppm

OTHER MEASUREMENTS 6.88 Fluoride(F)

Field Temp(C)

1.18 por

•	Mer	4	Tρ	45	Rge	22	Sec 14 Led 11			
Lab no: Index no: Well depth Water leve Top open i Bottom ope Altitude(f Bedrock el TDS(mg/l) Field Cond Field pH	inte inte in i	t) rval inter	(ft)	40 (t)	1033 4522 83.0 30.0		Date sampled Date submitted Date enalysed(major) Date analysed(minor) Sampled by Sample Source Owners name Hardness(as CaCO3) Alkalinity(as CaCO3) Cond(micromhos/cme25C) Lab pH	27 3 V0	GW 1 DSW 550 20	78 79 LL 172 ND •4 80
							•			. 5

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3)	mg/1 229.0 75.0 179.0 7.5 0.0 688.0	meq/1 11.43 6.17 7.79 0.19 0.00 11.28	f total anion or cation 44.7 24.1 30.4 0.8 0.0 43.4
Sulphate (SO4) Chloride (Cl) Nitrate (NO3) Hydroxide (OH) Silica (SiO2) Calcium (Acid) Magnesium (Acid) Calculated TDS	699.0 4.0 3.0 10.4 235.0 74.0 1545.2	14.55 0.11 0.05 Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	56.0 0.4 0.2 25.991 25.578 1.

MINOR CONSTITUENTS

Iron

7.7 ppm

OTHER MEASUREMENTS 5.70 Fluoride(F)

Field Temp(C)

0.10 ppm

	Mer	4	Tp	45	Rge	22	Sec 14	Lad 11	ı	
Lab no. Index no. Well dept Water let Top open Bottom op Altitude(Bedrock e TDS(mg/!) Field Con Field pH	h(f) fnte ion i ft)	ft) erval inter	val (í (ft)	40 't)	81051 4522 83.0 28.5 72.0 82.0		Date samp Date subm Date anal Date anal Sample So Owners na Hardness (Alkalinit Cond (migr Lab pH	nftted yeed(maj yeed(min yeed ource me as CaCO3 y(as CaC	01 lor) 5 lor) R v	11 78

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(C1) Nitrate(NO3) Hydroxide(OH) Siliga(SiD2)	mg/l 191.0 79.0 184.0 7.1 0.0 493.0 778.0 2.0 0.3	9.53 6.50 8.00 0.18 0.00 8.05 16.20 0.06	of total anion or cation 39.4 26.8 33.0 0.7 0.0 33.2 66.5 0.2 0.0
Calcium(Acid) Megnesium(Acid) Calculated TDS	231.0 69.0 1497.0	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	24.340 24.218 0.

MINOR CONSTITUENTS

Iron

10.2 ppm

OTHER MEASUREMENTS 7.80 Fluoride(F)

9.00 00=

М	# r	4	Tp	45	Rge	22	Sec 14 - Led 11		
Leb no. Index no. Well depth Water leve Top open in Bottom open Altitude(f) Bedrock ele TDS(mg/l) Field Cond(Field pH	i(dintention)	ft) Prva Inte	rval(f n(ft)	40 t)	1052 4522 83.0 28.5 72.0 82.0		Date sampled Date submitted Date analysed(major) Date analysed(minor)	VOGW 1 DS V E 745 346 17	78 79 79 ILL NT3 END

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(Cl) Nitrate(NO3) Hydroxide(OH) Silica(8102)	mg/1 167.0 80.0 185.0 7.1 0.0 425.0 778.0 2.0 2.6	meq/ 8.33 6.58 8.05 0.18 0.00 6.97 16.20 0.06 0.04 Total enions(epm)	of total anion of cation 36.0 28.4 34.8 0.8 0.0 29.9 69.6 0.2 0.2
Calcium(Acid) Magnesium(Acid) Calculated TDS	228.0 68.0 1444.9	Total cations(epm) Ion balance error(%) TDS balance error(%)	23,263 23,146 0, -10,

MINOR CONSTITUENTS

Iron

4 6.6 nnm

> OTHER MEASUREMENTS 6.38 Fluoride(F)

0.00 ppm

Field Temp(C)

AT .	8 P	4	Tp	45 Rge	22	Sec 14 Led 11	
Leb no. Index no. Well depth Water leve Top open i Bottom ope Altitude(f Bedrock el TDS(mg/!) Field Cond Field pH	it)	t) nva nte	nval(fi n(ft)	1700 -		Owners Source	D M Y 6 12 78 8 12 78 9 1 79 VOGWILL DSWT4 30 MINS 875.3 544.8 2070 7.8

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potessium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(\$04) Chioride(CI) Nitrate(NQ3) Hydroxide(OH)	mg/1 237.0 69.0 188.0 6.7 0.0 681.0 748.0 6.0	meq/i 11.83 5.68 8.18 0.17 0.00 11.16 15.57 0.17	of total anion or cation 45.7 22.0 31.6 0.7 0.0 41.5 57.9 0.6 0.0
Silica(SiO2) Calcium(Acid) Magnesium(Acid) Calculated TDS	17.4 216.0 72.0 1607.0	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	26.907 25.854 2. =7.

MINOR CONSTITUENTS

Iron

11 ppm

OTHER MEASUREMENTS 6.50 Fluoride(F)

0.10 ppm

Field Temp(C)

	Mer	4	Tp.	45	Rge	22	Sec 14 Led 1	1		
Lab ng. Index no. Well dept Water lev Top open Bottom op Altitude(Bedrock e TDS(mg/l) Field ph	h(f) en } ft)	rval nter	ve1 (1 (fe)	40 t)	1067 4522 84.0 30.0 72.0 82.0		Date sampled Date submitted Date submitted Date analysed(me) Sampled by Sample Source Owners name Hardness(as CaCO: Alkalinity(as Cat Cond(migromhos/gn	Jor) 9 nor) ((3)	12 12 1 DSW DSW 798 468	78 78 79 LL 174 ND

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chioride(C1) Nitrate(NO3) Hydroxide(OH) Silica(SiO2)	mg/1 203.0 71.0 188.0 6.3 0.0 586.0 778.0 8.0	meq/ 10.13 5.84 8.18 0.16 0.00 9.60 16.20 0.23 0.00	f total anion or cation 41.7 24.0 33.6 0.7 0.0 36.9 62.2 0.9
Calcium(Apid) Magnesium(Apid) Calculated TDS	13.9 244.0 70.0 1556.6	Total anions(epm) Total cations(epm) Ion belance error(%) TDS belance error(%)	26,034 24,312 3, =3,

MINOR CONSTITUENTS

Iron

6.4 000

OTHER MEASUREMENTS Fluoride(F)

Field Temp(C)

8.10 pom

	Mer	4	Tp	45	Rge	22	8ec	14	Lad	11			
Lab no. Index no. Well dep Water le Top open Bottom oi Altitude Bedrock of TDS(mg/): Field Cor Field pH	th(formal)	ft) prval Inter itior	vol(i	40 (t)	1077 4522 83.0 30.0 72.0 82.0		Date Samp! Samp! Owner Hardn Alka!	submined by e South seas (e inity migro	itted /sed(m /sed(m /ree /ree /rec /rec /rec	03) ec03) cm=25C	15 9 V0	12 12 1 0 0 1 0 1 1 1 1 1 1	78 79 LL 175 NS

MAJOR CONSTITUENTS

		. % o	f total anion
Calcium(Ca)	mg/1 232.0	ग व प्∕ ।	or cation
Maghas tum (Mg)	74.0	11.58	44.5
Sodium (Na)	188,0	6.09 8.18	23.4
Potassium(K) Carbonate(CO3)	6.7	0.17	31.4 0.7
Bicarbonate(HCO3)	0.0	0.00	0.0
Sulphate(804)	642.0 728.0	10.52	40.8
Chlorida (C1)	4.0	15.16 0.11	58,8
Nitrate(NO3)	0.2	0.00	0.4 0.0
Hydroxide(OH) 8111ge(8102)	44.0	·	
Calctum(Actd)	14.0 228.0	Total anions(epm)	25,796
Magnesium (Acid)	76.0	Total cations(epm) Ion belance error(%)	26,016
Calculated TDS	1562.6	TDS belance error(%)	0. =2.

MINOR CONSTITUENTS

Iron

11.7 ppm

OTHER MEASUREMENTS 7.78 Fluoride(F)

0.10 ppm

Field Temp(C)

	Mer	4	Īρ	45	Rge	22	Sec	14	Lad	11			
Lab no. Index no. Well dept Water lev Top open Bottom op Altitude(Bedrock e TD8(mg/l) Field Con Field pH	h(f) into	it) prvai Inter ition	(fe)	40 (t)	1078 4522 83.0 30.0 72.0 82.0		Date Date Samp Samp Owner Hardr Alkal	anali anali led by le Sours namess (a linity	itted ysed(m ysed(m yrce ne csCaC	(nor)	15 9 V	12 12 1 0GWI 08W 952 569	78 79 LL 175 ND

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potessium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(804) Chioride(C1)	mg/1 253.0 78.0 188.0 5.8 0.0 712.0 743.0 4.0	meq/1 12.62 6.42 8.18 0.15 0.00 11.67 15.47 0.11	of total anion or cation 46.1 23.5 29.9 0.5 0.0 42.6 56.8
Nitrate(NQ3) Hydroxide(OH)	0.3	0.00	0.4 0.0
Silice(SiO2) Celcium(Acid) Magnesium(Acid) Celculated TDS	14.0 236.0 75.0 1636.2	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	27.257 27.370 0. -5.

MINOR CONSTITUENTS

Iron

8,3 ppm

OTHER MEASUREMENTS 6.48 Fluoride(F)

8.18 ppm

Field Temp(C)

Мфр	4	Tp	45	Rge	22	Seç	14	Ls	đ	11			
Leb no. Index no. Well depth(fill Weter level(fill Top open into Bottom open Altitude(ft) Bedrock eleve TD8(mg/l) Field Cond(mi	it) erval inter etion	cfe)	40 2 ft)	1030 4522 40.0 30.0		Date Sampi Sampi Owner Hardr	ana ed t e So essi	nitte yeed yeed yeed yeed yeed as C((m (m	ejor) inor) 03) eCO3) em#25C	27 3 V(11 1 13CW 13CW 15MJ 134 587	NT1 INS I.9

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(804) Chloride(C1) Nitrate(NO3)	mg/! 30.0 14.6 470.0 2.5 0.0 734.0 448.0 10.0 1.8	meq/l 1.50 1.20 20.44 0.06 0.00 12.03 9.33 0.28	f total anion or cation 6.5 5.2 88.1 0.3 0.0 55.5 43.0 1.3
Hydroxide(OH) 811ica(\$102) Calcium(Acid) Magnesium(Acid) Calculated TDS	5.4 50.0 15.3 1344.2	Total enions(epm) Total cations(epm) Ton balance error(%) TDS balance error(%)	21.669 23.206 3.

MINOR CONSTITUENTS

Iron

9.1 ...

OTHER MEASUREMENTS

Field Temp(C)

0.50 ppm

Mer 4	Tp 45	Rge	55	Sec 14	Led 11			
Lab no. Index no. Well depth(ft) Water level(ft) Top open interval Bottom open inter Altitude(ft) Bedrock elevation TDS(mg/l) Field Cond(microm	(ft) vel(ft) (ft)	1031 4522 40.0 30.0		Date ana; Sampled b Sample So Owners na Hardness(Alkalinit	itted ysed(major) ysed(minor) y urce	27 3 VI 45	GW 1 3 S C W 3 O M 1 2 8 9 6 1 1	78 79 [LL NT1 INS

MAJOR CONSTITUENTS

		X (of total anion
a	mg/1	meq/1	or cation
Calcium(Ca)	73.0	3.64	
Magnestum (Mg).	26.0		16,8
Sodium (Na)		2,14	9.8
	365.0	15,88	73.1
Potassium(K)	2.9	0.07	
Carbonate(CO3)	9.0	• • • • • • • • • • • • • • • • • • • •	0.3
Bigarbonate (HCO3)		0.00	0.0
aldelindudta (UCD2)	764,0	12.52	59.7
Sulphate(SO4)	391.0	8.14	
Chloride(C1)	10.0	· · · · · · · · · · · · · · · · · · ·	38.8
Nitrate(NO3)	_	0,28	1.3
Huston I & Cours	2.0	0.03	0.2
Hydroxide(OH)		•	
\$111ce(\$102)	7,8	Total and sunday to	
Calajum (Agid)		Total anions(epm)	20.978
	71.0	Total cations(epm)	21,733
Magnestum (Agid)	25.0	Ion belance error(%)	
Calculated TDS	1253.4	The believe error(A)	
	. 20087	TDS belance error(X)	-10.

MINOR CONSTITUENTS

Iron

1 4 ---

Field Temp(C)

OTHER MEASUREMENTS 6.50 Fluoride(F)

9.50 pom

	Men	4	Τp	45	Rge	22	Sec	14	LsJ	1 1			
Lab no a Index no well dept water les Top open Bottom or Altitude (Bedrock et TDS(mg/1) Field Con Field ph	th(five)() into en (ft)	ft) erval inter	rval(i	40 2 ft)	31037 34522 340.0 30.0		Date and Date and Sample Sample Sample Alkali Cond (m	Bubmala Brala Brala Bras Bras Bras Bras Bras Bras Bras Bra	itted /**d(! /*ed ! / / / / / / / / / / / / / / / / / / /	major) mino CO3) CaCO3)	27 3 V(11 11 13 35 C M 10 M J 20 J 61 6	78 79 ILL 112 INS

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(804) Chloride(C1)	mg/1 53.0 17.3 475.0 2.9 0.0 771.0 520.0	meq/1 2.64 1.42 20.66 0.07 0.00 12.64 10.83	f total anion or cation 10.7 5.7 83.3 0.3 0.0 53.6 45.9
Nitrate(NO3) Hydroxide(OH) Silica(SiO2) Calcium(Acid) Magnesium(Acid) Calculated TDS	4.0 0.0 10.3 57.0 17.9	0.11 0.00 Total anions(epm) Total cations(epm) Ion belance error(%)	0.5 0.0 23.577 24.804 3.
· · · · · · · · · · · · · · · · · · ·	1461.6	TDS balance error(%)	1.

MINOR CONSTITUENTS

Iron

r)

8.7 000

OTHER MEASUREMENTS 5.25 Fluoride(F)

Field Temp(C)

8.50 00

Mer 4	1p 4	5 Rge	22 Sec	14 Lsd 11	
Lab no. Index no. Well depth(ft) Water level(ft) Top open interv Bottom open int Altitude(ft) Bedrock elevati TDS(mg/1) Field Cond(micr Field pH	al(ft) enval(ft on(ft)	1348.0	Date Date Samp Samp Owne Hard Alka	sampled submitted analysed(major) analysed(minor) led by le Source rs name ness(as CaCO3) [inity(as CaCO3) (micromhos/cme25C)	D M Y 21 11 78 27 11 78 4 1 79 VOGWILL BSCWT2 END 317.3 599.2 1880 7.2

MAJOR CONSTITUENTS

			of total anion
Calabaran	mg/1	meq/1	or cation
Calclum(Ca)	81.0	4.04	18.1
Magnestum(Mg)	28.0	2.30	10.3
Sodium(Na)	365.0	15.88	-
Potassium(K)	2.9	-	71.2
Carbonate(CO3)	-	0.07	Ø.3
	1.7	<i>। 🙀 भी 🐶</i>	Ø . Ø
bicarbonate(HCO3)	749.0	12.28	57.2
Sulphate(SO4)	428.2	8.91	41.5
Chloride(Cl)	8.0	Ø.23	_
Nitrate(ND3)	2,5		1.1
Hydroxide(OH)	F # 3	0.04	0.2
Silica(SiD2)	9.7	Total anions(epm)	21.454
Calcium(Acid)	79•0	Total cations(epm)	22,297
Magnesium(Acid)	27.0	Ion balance error(%)	-
Calculated TDS	1293.4		
	1273.4	TDS balance error(%)	-4 ,

MINOR CONSTITUENTS

Iron

2.2 ppm

OTHER MEASUREMENTS 5.50 Fluoride(F)

Men 4	Tp 45	Rge 22	Sec 14	Lad 11		
Leb noe Index noe Well depth(ft) Weter level(ft) Top open intervel Bottom open intervel Altitude(ft) Bedrock elevation TDS(mg/l) Field Cond(microm) Field pH	404 24 (ft) val(ft) 24 (ft)	1049 4522 40.0 31.5 7.0 10.0	Date anal Sampled be Sample Somers named Hardness (Alkalinity	itted ysed(mejor) ysed(minor) y urce	28 1 01 1 4 R VOG BS 30 21	

MAJOR CONSTITUENTS

	m = 41	X :	of total anion
Colodinators	mg/1	meq/1	or cation
Calclum(Ca)	66.0	3,29	13,3
Magnestum(Mg)	21,1	1.74	-
Sodium(Na)	453.0		7.0
Potassium(K)		19.70	79,5
	17	0.04	0.2
Carbonate(CO3)	0.0	0.00	0,0
Bicarbonate(HCO3)	715.0	11,72	51.8
\$uiphate(\$04)	512.0	10.66	
Chloride(C1)	8.0		47,2
Nitrate(NO3)		0,23	1.0
	0.0	0.00	0.0
Hydroxide(OH)			•
.\$111ca(\$102)	8.5	Total anions(epm)	22,605
Calcium(Acid)	63,0		
Magnesium (Acid)		Total cations(epm)	24,778
	21.1	Ion balance error(%)	5.
Calculated TDS	1421.9	TDS balance error(X)	-10.

MINOR CONSTITUENTS

Iron

8.8 000

field Temp(C)

OTHER MEASUREMENTS 5.60 Fluoride(F)

0.40 ppm

M	er	4	Ţρ	45	Rge	22	Sec	14	Lsd	1 1			
Lab no. Index no. Well depth Water leve Top open i Bottom ope: Altitude(f Bedrock ele TDS(mg/1) Field Cond Field pH	l(intententententententententententententen	t) erval nter	(ft)	40 2 t) 2	1050 4522 40.0 31.6 97.0 40.0		Date Date Sampl Sampl Owner Hardr Alkal	submanal anal ed be So na ess(init	itted ysed(may ysed(may urce	inor) R 03) 2003).	28 91 4 VOG B	12 1 WIL SCW E 229 528 18	78 78 79 L T3 ND .3

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K)	mg/1 49.0 26.0 371.0 2.1	mea/1 2.45 2.14 16.14	of total anion or cation 11.8 10.3 77.7
Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(Cl) Nitrate(NO3) Hydroxide(OH)	0,0 661.0 502.0 8.0 0.1	0.00 10.83 10.45 0.23 0.00	0,0 50.4 48.6 1.0 0.0
Stlica(SiO2) Calcium(Acid) Magnesium(Acid) Calculated TDS	8.6 78.0 25.0 1291.8	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	21.513 20.776 2.

MINOR CONSTITUENTS

Iron

3.4 ppm

OTHER MEASUREMENTS 6.40 Fluoride(F)

	Mgn	4	Τp	45	Rge	22	Sec	14	Led	11				
Lab no. Index no. Well dept Water lev Top open Bottom op Altitude(Bedrock e TDS(mg/l) Field Conc Field pH	h(fi e)(fi inte en i ft)	t) rval nter	(ft)	40 2 (t) 2	1064 4522 40.0 30.0 90.0 40.0		Date Date Date Samp Samp Owner Hardr	samp subm analy analy led by le Source re nem ress(e) inity	led itted ysed(n ysed(n urge ne es (e)	mejor) minor)	8 5 VC 8 32	12 12 1 1 1 1 1 1 1 1 2 1 5 8 4 1 2 1 2 1 2	78 79 ILL 114 INS	·

MAJOR CONSTITUENTS

	4.4	. x	of total anion
0-1 1 45 3	mg/1	meq/1	or cation
Calcium(Ca)	61.0	3.04	
Magnes (um (Mg)	16.0		12.1
Sod um (Na)	_	1.32	5.2
ODGIGMENAN	476.0	20.70	82.2
Potassium(K)	4.2	0.11	
Carbonate(CO3)	-	•	0.4
	0.0	0.00	0.0
Bicarbonate(HCO3)	730.0	11,97	49.9
Sulphate(SO4)	564.0		
Chloride(C1)	•	11,74	48,9
	10.8	0.28	4 1.2
Nitrate(NO3)	0.1	0.00	0.0
Hydroxide(OH)	•	2400	0.0
8111ca(8102)	0.5	.	
	9,5	Total anions(epm)	23,992
Calcium(Acid)	61.0	Total cations(epm)	
Magnesium (Acid)	16.0	Too helenes seems seems	25,173
Calculated TDS	-	Ion belence error(%)	2.
caindiated 100	1499.7	TDS belence error(%)	-12.

MINOR CONSTITUENTS

Iron

7.3 ppm

OTHER MEASUREMENTS 6.20 Fluoride(F)

Field Temp(C)

0.50 pp:

Mer 4	Γ ρ 4	5 Rge	22	Sec 14 Led 11			
Leb no. Index no. Well depth(ft) Water level(ft) Top open interval(f	't)	781065 404522 240.0 30.0 30.0		Date sampled Date submitted Date analysed(major) Date analysed(minor) Sampled by	5 1 8 1 5	2 1 1 WI	78 79 LL
Altitude(ft) Bedrock elevation(ft) TDS(mg/l) Field Cond(migromho Field pH	t)	1282.0		Sample Source Owners name Hardness(as CaCO3) Alkalinity(as CaCO3) Cond(migromhos/cme25C) Lab pH	1 4	75 82 17	ND .2 .3

MAJOR CONSTITUENTS

4		· * * * * * * * * * * * * * * * * * * *	f total anion
6-1 1 4-1	mg/1	meq/	or cation
Calcium(Ca)	29.0	1.45	
Magnes ium (Mg)	25.0	· ·	7.2
	- -	2.06	10.2
Sodium(Na)	381.0	16,57	
Potassium(K)	3.3	- C30	82.2
Carbonate(CO3)		0.08	0.4
	14.4	0.48	2.5
Bicerbonete (HCO3)	573.0	9,39	
Sulphete(504)	450.0		48.1
Chioride (C1)	-	9.37	48,0
411011041617	10.0	0.28	1.4
Nitrete(NO3)	9.0	0.00	
Hydrexide(OH)			0.0
8414/84001			
3111qa(8102)	9.0	Total anions(epm)	19.523
Calcium(Acid)	79.0	Total contents	
Magnestum (Agid)	_	Total cations(epm)	20,162
	25.0	Ion belance error(%)	2.
Calculated TDS	1203.4	TDS balance error(%)	•
		ind nationed attock?	• 6.

MINOR CONSTITUENTS

Iron

2.3 ppm

Field Temp(C)

OTHER MEASUREMENTS 6.20 Fluoride(F)

8,50 ppm

Mer	4	1p	45	Rge	22	Sec	14	Lsd	11			
										D	M	Y
Lab no.			78	1074		Date	samp	ed		12	12	78
Index no.			40	4522		Date	submi	tted		13	12	78
Well depth(f	t)		24	40.0		Date	analy	sed(r	major)	9	1	79
water level(ft)		Ç	30.0		Date	analy	sed(ninor)			
Top open int	erva	l(ft)	ç	0.00		Samp	led by	/		٧¢	IGH !	[LL
Bottom open	inte	rval(f	t) 24	40.0		Sampl	e Sou	rce		F	SC	N T 5
Altitude(ft)						Owner	s nam	n e		3	BOM!	INS
Bedrock elev	ation	i(ft)				Hardr	ess(a	s Ca(:03)		228	3.0
TDS(mg/1)			147	74.0		Alkal	inity	(as (CaC03)		628	8,6
Field Cond(m	icrof	nhos/c	m)			Cond	micro	mhos	/cm#250)	20	390
Field pH						Lab p	Н				7	7.7

MAJOR CONSTITUENTS

		4 0	r total anion
	m 🔅	meq/l	or cation
Calcium(Ca)	65	3,24	13.0
-Magnesium(Mg)	16	1 . 2	5,3
Sodium(Na)	465	20 3	81.4
Potassium(K)	5.9	9.47	0.3
Carbonate(CO3)	0.0	0.00	0.0
Bicarbonate(HCO3)	786.0	12.88	51.5
Sulphate(SO4)	563.0	11.72	46.9
Chloride(C1)	14.0	ย.39	1.6
Nitrate(NO3)	Ø • 1	0.00	0.0
Hydroxide(OH)		1)	
Silica(SiO2)	10.4	Total anions(epm)	25,001
Calcium(Acid)	66.0	Total cations(epm)	24.861
Magnesium (Acid)	21.0	Ion balance error(%)	0.
Calculated TDS	1522.9	TDS balance error(%)	3.

MINOR CONSTITUENTS

Iron 8.6 ppm

OTHER MEASUREMENTS 5,20 Fluoride(F)

Field Temp(C)

0.40 ppm

M	4p 4	Tp	45	Rge	5 2	Sec 14 Lad 11			
Leb no. Index no. Hell depth Heter leve Top open in Bottom open Altitude(f) Bedrock ele TDS(mg/l) Field Cond((†¢) i(†¢) ntorval n inter k) avation	(ft)	46 2 (t) 2	31076 34522 340.0 30.0 90.0 40.0		- 11888 4 41.64.14.4	15 9 VO 8	GW1 8CW 513 624	78 79 LL 175 ND

MAJOR CONSTITUENTS

Celcium(Ca) Magnesium(Mg) Sodium(Na) Potessium(K) Cerbonete(CO3) Bicerbonate(HCO3) Sulphate(SO4) Chloride(C1) Nitrete(NO3) Hydroxide(OH)	mg/1 81.0 27.0 390.0 2.5 0.0 781.0 437.0 10.0	meq/1 4.04 2.22 16.96 0.06 0.00 12.80 9.10 6.28 0.00	of total anion or cation 17.4 9.5 72.8 0.3 0.0 57.7 41.0 1.3 0.0
Silica(SiO2) Calcium(Acid) Megnealum(Acid) Calculated TDS	10.5 79.0 26.0 1342.1	Total anions(epm) Total cations(epm) Ion belance error(x) TOS balance error(X)	22.183 23.292 2. 6.

MINOR CONSTITUENTS

Iron

3.1 ppm

OTHER MEASUREMENTS

6.50 Fluoride(F)

8.58 com

Ploid Temp(C)

	Men	4	Tp	45	Rge	5 2	Seç	14	Lad	11			
Leb no. Index no. Well dept Weter let Top open Bottom or Altitude Bedrock e TDS(mg/l) Field Cor Field pH	+ († ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	it) rvai nter	(ft)	* 80 2 (t) 2	40.0 29.3 90.0		Date Date Date Samp Samp Hardr Alka	sempi submi enally enally e South e So	ied itted ysed(n ysed(n urce ne ss (as	nejor) ninor)	20 3 R V0 NE	PIL PIL WS1 22 498	78 79 LL OT ED

MAJOR CONSTITUENTS

		* (of total anion
Caladyadaa	mg/1	meq/1	or cation
Calcium(Ca)	6.1	0.30	1.6
Magnesium (Mg).	1.7	0.14	
Sodium(Na)	419.0		8.7
Potassium(K)	· -	18.23	97.1
Carbonate(CO3)	4.2	0.11	0.6
	19.2	0.64	3,6
Biserbonate(HCO3)	573.0	9.39	53,2
Sulphate(804)	337.0	7.02	
Chloride (C1)	16.0		39,7
Nitrate (ND3)	10.1	0.45	2,6
Hydrox (de (OH)	10.1	0,16	0.9
Gilia-tology			
3111ce(8102)	2,4	Total anions(epm)	17,662
Colatum (Asid)	314.0	Total cations(epm)	18,777
Magnestum (Acid)	99.0	Ton holonge concerts	▼ 33
Calculated TDS	1097.4	Ion belence error(%)	
	/ . 4	TDS balance error(%)	-10.

MINOR CONSTITUENTS

Iron 59 ppm

OTHER MEASUREMENTS Fluoride(F)

0.80 ppm

Mer	4	Τp	45	Rge	22	Sec 14 Lad 11			
Lab no. Index no. Well depth(fit) Water level(fit) Top open inter Bottom open inter Altitude(ft) Bedrock eleva TDS(mg/l) Field Cond(mit) Field pH	it) rvai nter	vel (1 (ft)	B01 24 (t) 24	40.0		Date sampled Date submitted Date enalysed(major) Date analysed(minor) Sampled by Sample Source Owners name Hardness(as CaCO3) Alkalinity(as CaCO3) Cond(micromhos/cme25) Lab pH	20 3 R. V(1	11 11 1 10 10 10 10 10 10 458 18	78 79 LL IN ED

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(C1)	mg/1 32.0 26.0 388.0 3.8 .0.0 573.0 438.0	meq/1 1.60 2.14 16.88 0.10 0.00 9.39 9.12	of total anion or cation 7.7 10.3 81.5 0.5 0.0 50.0 48.5
Nitrate(NO3) Hydroxide(OH)	8.0	0.23 0.06	1.2
Silica(SiD2) Calcium(Acid) Magnesium(Acid) Calculated TDS	5.9 83.0 30.0 1187.3	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	18.800 20.711 5.

MINOR CONSTITUENTS

Iron

9.3 ppm

OTHER MEASUREMENTS Fluoride(F)

0.50 ppm

بين منها. الله

Mer 4 Tp 48	Rgë	22	Sec	14	Lad	11			
							D	M	Y
Lab no.	781024		Date	sampl	ed		16	11	
Index no.	BOHWT1 :			submi				11	
Well depth(ft)	240.0					nejor)		1	
Water level(ft)	29.3					inor)		•	•
	90.0			ed by			R V) GW 1	111
Bottom open interval(ft)	240.0			. 304				30 N	
Altitude(ft)	-			s nem				WSI	
Bedrock elevation(ft)					-	:03)			3.9
TDS(mg/1)	1512.0					aC03)		636	•
Field Cond(micromhos/cm)	8		Cond (micro	mh0#/	cm#25	C) .		50
Field pH			Lab p	Н				7	. 8

MAJOR CONSTITUENTS

		X •	f total anion
	mg/1	meq/	or cation
Calcium(Ca)	24.0	1.20	4.9
Magnesium (Mg)	5.1	0.42	1,7
Sodium(Na)	520.0	22.62	93.1
Potassium(K)	2,5	0.06	0.3
Carbonate(CO3)	0.0	0.00	
Bicarbonate (HCO3)	795.0		0.0
	-	13,03	54.7
Sulphate (804)	500.0	10.41	43,7
Chionide (C1)	14.0	0.39	1.7
Nitrate(NO3)	0.0	0.00	0.0
Hydroxide(OH)	, •		
S111ca(8102)	6.7	Total enfons(epm)	23.836
Calcium(Acid)	25.0	Total cations(epm)	24.300
Magnestum (Acid)	6.0	Ion balance error(%)	241000
Calculated TDS			<u>.</u> •
anifelated (DD	1463.2	TDS belence error(%)	-3.

MINOR CONSTITUENTS

Iron

2.6 ppm

OTHER MEASUREMENTS 6.30 Fluoride(F)



8.48 000

ı	401	4	Tp	45	Rge	2 2	Sec	14	Led	11			
Lab nee Index noe Well depth Water leve Top open i Bottom ope Altitude(f Bedrogk el TD\$(mg/l) Field Cond	nt (ft) Prval Inter	(ft)	80 2 t) 2	1025 HWT1 40.0 29.3 90.0 40.0		Date Date Date Sampi Sampi Owner Hardr	analy analy ed by e Source s nam ess(a inity	itted ysed(m ysed(m yrce ne ss CaC	03) cm=25	20 3 R VC NE	11 11 1 1 1 1 1 1 1 2 3 6 6 7 1 8	78 79 ILL ND TED

MAJOR CONSTITUENTS

		X 0	f total anion
0.1-1.40-2	mg/1	meq/1	or cation
Calcium(Ca)	49.0	2.45	
Magnes (um (Mg)	19.8		11.8
Sodium(Na)		1,63	7.9
O O G T G M (N A)	379.0	16.49	79.9
Potassium(K)	2.9	-	
Carbonate(CO3)		0.07	0.4
	0.0	0.00	0.0
Bicarbonate(HCO3)	759.0	12,44	64,3
Sulphate(\$04)	311.0		
Chloride (C1)		6,48	33.5
	14.0	0.39	2.0
Nitrate(NO3)	2.4	0.04	
Hydroxide(OH)	, ·		0.2
Silica(3102)	• •		
	5 • 8	Total anions(epm)	19.349
Calelum (Aeld)	58.9	Total cations(epm)	
Magnesium (Agid)	21.6		20,634
Calculated TDS		Ion belance error(x)	3.
-4.44.4/40 103	1157.1	TD8 belence error(%)	-11.

MINOR CONSTITUENTS

Iron 6.8 ppm

OTHER MEASUREMENTS 5.50 Fluoride(F)

Field Temp(C)

0.70 pom

Mer 4	Tp 45	Rge 22	Sec 14 Lsd 11	
				D M Y
Lab no.	781	036	Date sampled	23 11 78
Index no.	484	522		27 11 78
Well depth(ft)	2.4	0.0	Date analysed(major)	3 1 79
Water level(ft)	3	0.0	Date analysed(minor)	
Top open interval	(ft) 9	7.0	Sampled by	VOGWILL
Bottom open inter	val(ft) 24	0.0	Sample Source	BOHWT2
Altitude(ft)			Owners name	BUMINS
Bedrock elevation	(ft)		Handness(as CaCO3)	136.7
TDS(mg/1)	123	4.0	Alkalinity(as CaCO3)	630.4
Field Cond(microm	hos/cm)		Cond(micromhos/cme250)	1832
Field pH			Lab pH	7,8

MAJOR, CONSTITUENTS

		%	of total anion
	mg/1	mea/1	or cation
Calcium(Ca)	36.0	1.80	8.4
Magnesium(Mg)	11.4	0.94	4.4
Sodium(Na)	430.0	18.70	87.1
Potassium(K)	1.7	0.04	0.2
Carbonate(CO3)	0.0	0 • ØØ	0.0
Bicarbonate(HCO3)	788.0	1.2.92	59.0
Sulphate(\$04)	383.0	7.97	36.4
Chloride(C1)	36,0	1,02	4.6
Nitrate(NO3)	0.1	0.00	0.0
Hydroxide(OH)			•
Silica(SiO2)	9.6	Total anions(epm)	21.907
Calcium(Acid)	38.0	Total cations(epm)	-
Magnestum(Acid)	12.3	Ion balance error (%) 1.
Calculated TDS	1295.3	TDS balance error(

MINOR CONSTITUENTS

Iron 6.6 ppm

OTHER MEASUREMENTS 6.00 Fluoride(F)

	Men	4	Tp	45	Rge	22	8ec	14	Led	11			
Lab no. Index no.	ı				1058 4522		Date		led itted			M 11	78
Well dept Water lev Top open	h(f)	iti	(fe)	2	40.0 29.3 90.0		Date	anal	ysed(n	najor) ninor)	5		79
Bottom op Altitude (Bedrock e	en (nter	val(ft) 2	40.0		Samp! Owner	e 80	urce me		6		NT2
TDS(mg/j) Field Con Field pH		88		12 em)	42.0		Alkal	init	y(as C	03) aCO3) cm#25			-

MAJOR CONSTITUENTS

	4.	W X (of total anion
	mg/1	meq/1	or cation
Calclum(Ca)	25.0	1,25	6.4
Magnesium(Mg)	20.0	1.65	8,4
Sodium(Na)	381.0	16.57	84.8
Potassium(K)	3.3		-
		0.08	0.4
Carbonate(CO3)	12.0	0.40	2,2
Bicarbonate (HCO3)	610,0	10.00	53.9
Sulphate(SO4)	383.0	7.97	43,0
Chloride(Cl)	6.0	0.17	0.9
Nitrate(ND3)	1.4	0.02	0.1
Hydroxide(OH)	• •		0.1
Silica(SiO2)	9.1	Total anions(epm)	18.564
Calcium(Acid)	63.0		
	· -	Total cations(epm)	19.550
Meanestum (Agid)	19.0	Ion balance error(%)	3.
Calculated TDS	1140.7	TDS balance error(%)	

MINOR CONSTITUENTS

Iron

2.7 ppm

OTHER MEASUREMENTS 7.90 Fluoride(F)

Field Temp(C)

Mer 4 Tp	45 F	Rge 22	Sec 14 Led 11		
Lab no. Index no. Well depth(ft) Water level(ft) Top open interval(ft Bottom open interval Altitude(ft) Bedrock elevation(ft TDS(mg/l) Field Cond(micromhos Field pH	(ft) 240.	22 , 0 , 3 , 0		BOHW 30 M 187 615	78 79 LL 173 11N

MAJOR CONSTITUENTS

2 *		· % o	f total anion
	mg/1	meq/1	or cation
Calcfum(Ca)	49.0	2.45	10.7
Magnesium(Mg)	15.8	1.30	
Sodium (Na)	436.0	18.96	5.7
Potassium(K)	3.8	- ·	83.2
	" -	0.10	0,4
Carbonate (CO3)	0.0	0.00	0.0
Bicarbonate (HCO3)	769.0	12.60	58.7
Sulphate(SO4)	398.0	8.29	38.6
Chloride(C1)	20.0	0.56	
Nitrate(NO3)	0.0	•	2.6
Hydroxide (OH)	0 0	0.00	0.0
S111ca(S102)		_	
	9.3	Total anions(epm)	21.455
Calcium (Acid)	77.0	Total cations(epm)	22.808
Magnesium (Acid)	15.0	Ion balance error(%)	3.
Calculated TDS	1310.0	TDS balance error(%)	
		A A A A A A A A A A A A A A A A A A A	-8 .

MINOR CONSTITUENTS

Iron

6.5 ppm

OTHER MEASUREMENTS 5.30 Fluoride(F)

0.70 pp

Field Temp(C)

	Mer	4	Tp	45	Rge	22	Sec 14 Ls	d 11				
Lab no. Index no Well deport Water lev Top open Bottom or Altitude Bedrock a TDS(mg/1) Field Cor Field pH	th(five)(finte Pen (ft) Pleye	ft) Prva Inte	rval(· n(ft)	40 2 ft) 2	1059 4522 40.0 30.0 90.0 40.0		Date sampled Date submitted Date analysed Date analysed Sampled by Sample Source Owners name Hardness(as Ca Alkalinity(as Cond(migromhos Lab pH	d (major) (minor) =CO3) C=CO3)	8 5 V(256 638 17	78 79 ILL 13 ND	

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(804) Chloride(C1) Nitrate(NO3) Hydroxide(OH) Silica(8102)	mg/1 68.0 21.0 381.0 2.9 0.0 788.0 334.0 16.0	meq/ 3.39 1.73 16.57 0.07 0.00 12.92 6.95 0.45 0.00	total anion or cation 15.6 7.9 76.1 0.3 0.0 63.6 34.2 2.2 0.0
Calcium(Acid) Magnesium(Acid) Calculated TDS	8.9 65.0 20.0 1219.3	Total anions(epm) Total cations(epm) Ton belance error(%) TDS balance error(%)	20.321 21.768 3. -3.

MINOR CONSTITUENTS

Iron

1.7 ...

OTHER MEASUREMENTS: 6.98 Fluoride(F)

Field Temp(C)

M	ler	4	Τρ	45	Rge	22	Sec	14	Lsd	11			
Lab no. Index no. Hell depth Water leve Top open i Bottom ope Altitude(f Bedrock el TDS(mg/!) Field Cond Field pH	nten i	t) nval nter	(ft)	40 2 (t) 2	1058 4522 40.0 30.0 90.0 40.0		Date Date Date Samp! Samp! Owner Hardn Alkal	analy ed by e Sou s nam ess(a inity migro	tted sed(n ree c c c c c c c c c c c c c c c c c c	03) (cm#25C)	8 9 V(6 3	GW] BOHW 174 601	78 78 79 LL 174 NS

MAJOR CONSTITUENTS

Calcium(Ca) Magnasium(Mg) Sodium(Na) Potassium(K) Carbonate(CO3) Bicarbonate(HCO3) Sulphate(SO4) Chloride(Cl) Nitrate(NO3)	mg/1 45.0 14.1 439.0 1.7 0.0 752.0 375.0 22.0	meq/ 2.25 1.16 19.10 0.04 0.00 12.33 7.81 0.62	of total anion or cation 10.0 5.1 84.7 0.2 0.0 59.4 37.6 3.0
Hydroxide(OH)	0.2	0.00	0,0
Silica(SiO2) Calcium(Acid)	10.0	Total anions(epm)	20.757
Magnesium(Acid)	45.0	Total cations(epm)	22,545
Calculated TDS	14,0 1276.8	<pre>Ion balance error(%) TDS balance error(%)</pre>	4. =5.

MINOR CONSTITUENTS

Iron

3.4 ppm

OTHER MEASUREMENTS 5,50 Fluoride(F)

0.70 por

Field Temp(C)

	Men	4	Τp	45	Rge	22	3ec	14	Led	11			
Lab no. Index no Well dep Water le Top open Bottom of Altitude Bedrock TDS(mg/) Field Cor Field pH	th(five)(five)	ft) erva Inter	rval(: n(ft)	40 2 ft) 2 12	1069 4522 40.0 30.0 90.0 40.0		Date Date Sampi Sampi Owner Hardn Alkal	aubmana! ana! ed b e So s na ess(init	oled itted ysed(ysed(ysed(ource me as Cat	major) minor)	13 9 Vi	277 628	78 79 LL 114 ND

MAJOR CONSTITUENTS

		x o	f total anion
6 1 1 40 1	mg/1	meq/1	or cation
Calcium(Ca)	75.0	3,74	
Magnesium(Mg)	22.0		16.7
		1.81	8.1
Sodium (Na)	385.0	16.75	-
Potassium(K)	2.9		74.8
Carbonate(CO3)		0.07	0.3
	0.0	0.00	0.0
Bicarbonate(HCD3)	786.0	12.88	
Sulphate (504)	348.0	·	62.8
Chloride(C1)		7,25	35,3
	14.0	0,39	1,9
Nitrate(ND3)	0.2	0.00	3 6
Hydroxide(DH)		0,00	0.0
Silica(SiO2)			
	9.8	Total anions(epm)	20.527
Calcium(Acid)	67.0	Total cations(epm)	
Magnesium(Agid)	22.0	intal carious (abm)	22,374
	_	Ion belance error(%)	4.
Calculated TDS	1243.4	TDS belence error(X)	-1

MINOR CONSTITUENTS

Iron

2.7 ppm

OTHER MEASUREMENTS 6,90 Fluoride(F)

Field Temp(C)

Men 4	Tp 45	Rge 22	Sec 14 Lsd 11			
Lab no. Index no. Well depth(ft) Weter level(ft) Top open interval Bottom open inter Altitude(ft) Bedrock elevation	78 40 2 (ft) val(ft) 2	1079 4522 40.0 30.0	Date sampled	V0(B(12	78 79 LL 175 NS
TDS(mg/1) Field Cond(microm Field pH	12((hos/em)	50.0	Alkalinity(as CaCO3) Cond(migromhos/cm#25C) Lab pH		534 18	

MAJOR CONSTITUENTS

		x o	f total anion
6 1 1 46 1	mg/1	meq/1	or cation
Calcium(Ca)	51.0	2,54	11.3
Magnes (um (Mg)	16.0	1.32	5.8
Sodium(Na)	429.0	18.66	_
Potassium(K)		· ·	82.7
	1.7	0.04	0.2
Carbonate(CO3)	.0 , 0	0.00	0.0
Bicarbonate (HCO3)	793.0	13.00	60.9
Sulphate(804)	368.0	7.66	
Chloride(C1)	24.0	•	35,9
		0.68	3.2
Nitrate(NO3)	0.3	0.00	0.0
Hydroxide(OH)		· •	
3111ca(3102)	10.1	Total anions(epm)	04 744
Calcium (Acid)			21,341
	50.0	Total cations(epm)	22.566
Magnestum (Actd)	17.3	Ion balance error(%)	3.
Calculated TDS	1290.0	TDS balance error(%)	2.

MINOR CONSTITUENTS

Iron

4.7 ppm

OTHER MEASUREMENTS 5.30 Fluoride(F)

Field Temp(C)

0.70 ppm

Mer 4	Tp 45	Rge	22	Sec 14	Lad 11			
Lab no. Index no. Well depth(ft) Water level(ft) Top open interval Bottom open interval Altitude(ft) Bedrock elevation TDS(mg/!) Field Cond(microm) Field pH	(fe) val (ft) (fe)	81088 04522 240.8 29.3 92.0 240.0		Date anal Sampled b Sample So Owners na Hardness(Alkalinit	itted yped(major; ysed(minor; y urce	04) 10) R V(12 01 1 30Hw 269 628	79 79 LL 15 ND .8

MAJOR CONSTITUENTS

		* 0	f total anion
0-1-1-1-10-1	mg/1	meq/1	or cation
Calcium(Ca)	60.0	2.99	•
Magnes um (Mg)	29.0		13.7
Sodium (Na)	379.0	2.39	10.9
Potassium(K)		16,49	75.2
	2,5	0.06	0,3
Carbonate (CO3)	.0.0	0.00	
Bigarbonate(HCO3)	786.0	12,88	0.0
Sulphate (804)	362.0		61.9
Chloride (C1)	_	7,54	36,2
	14.0	0.39	1.9
Nitrate(NO3)	0.0	0.00	0.0
Hydnoxide(OH)	_	7 4 6 5	0,0
Silica(SiO2) =	9.1	Takal auto at a	7 <u> </u>
Calcium (Acid)		Total enions(epm)	20,815
	66,0	Total cations(epm)	21.930
Magnestum (Açid)	25.0	Ion balance error(%)	3.
Calculated TDS	1242.1	TDS balance error(%)	
		. an maignes strock(V)	3.

MINOR CONSTITUENTS

Iron 2.2 pp

OTHER MEASUREMENTS 7.18 Fluoride(F)

Field Temp(C)

Men 4	Tp	45	Rge	22	Sec	14	Led	11			
									D	M	Y
Lab. no.		7818	35		Date	semp!	ed		20	11	
Index no.		4045	322			submi			27		•
Well depth(ft)		246	0.0			enely		nalor)	3	-	79
Water level(ft)		36	. 0			analy				-	
Top open interval(ft)	97	0			ed by		93	٧r	GW:	T 1 1
Bottom open interv	91(4					e Sou				OH	_
Altitude(ft)	• •					s nam				IOM :	
Bedrock elevation(663								•	-	
4001 (1)	1 1 2					088(a				157	, 9
TDS(mg/1)		1414	. 0		Alkal	inity	(88 (eCO3)		634	1.4
Field Cond(micromh)s/c	m)			Cond	micro	nhos/	cm=25C)			80
Field pH					Lab p	Н		•		7	9

MAJOR CONSTITUENTS

		X •	f total anion
	mg/1	meq/1	or cation
Calcium(Ca)	42.0	2.10	9.3
Magnesium (Mg)	12.9	1.05	4,7
Sodium (Na)	443.0	19.27	85,7
Potassium(K)	2.5	0.06	0,3
Carbonate(CO3)	0.0	0.00	0.0
Bicarbonate(HCO3)	793.0	13.00	
Sulphate(804)	408.0	· · · · · · · · · · · · · · · · · · ·	59.1
Chloride (Cl)	18.0	8.49	38,6
		0,51	2,3
Nitrate(NO3)	Ø . 5	0,01	0.0
Hydroxide(OH)		• •	▼ -
Silica(SiO2)	6,8	Total anions(epm)	22.008
Calcfum(Acid)	40.0	Total cations(epm)	22,491
Magnesium (Acid)	12.4	Ion balance error(%)	1.
Calculated TDS	1323.6	TDS balance error(%)	-6 ,

MINOR CONSTITUENTS

Iron 3.2 ppm

OTHER MEASUREMENTS 7.10 Fluoride(F)

Field Temp(C)

8.68 Des

Mer	4	Tp	45	Rge	22	Sec 14	i Li	ed 11			
Lab no. Index no. Well depth(#	(t)		40	1034 4522 40.0		Date se	bmitte		27	11	
Water level(Top open int Bottom open Altitude(ft)	ft) erval inter	(ft) val(i		30.0		Date an Date an Sampled Sample	alysed by Source	(mino	(n)	OGW Boh	AT1
Bedrock elev TDS(mg/1) Field Cond(m Field pH	ation	•	12! ;m)	56.0		Owners Hardnes Alkalin Cond(mi	s(as (Caco	3)	22 62 1	END 6.6 6.4 820 7.9

MAJOR CONSTITUENTS

		X (of total anion
0.1-1.40%	mg/1	meq/	or cation
Calcium(Ca)	56.0	2.79	13,4
Magnesium(Mg)	21.1	1.74	8,3
Sodium(Na)	373.0	16.22	
Potassium(K)	2.9	· · · · · · · · · · · · · · · · · · ·	77.9
Carbonate(CO3)		0.07	0.4
	0.0	0.00	0.0
Bicarbonate(HCO3)	783.0	12,83	64.0
Suiphate (\$04)	322.0	6.70	33,4
Chloride(C1)	18.0	0.51	2.5
Nitrate(ND3)	0.0	0.00	
Hydroxide(OH)		0,00	0 , 0
Silica(S102)	8.1	Total enions(epm)	80 046
Calcium (Acid)			20.046
	55.0	Total cations(epm)	20.830
Magnesium (Agid)	20.4	Ion balance error(%)	2.
Calculated TDS	1186.1	TDS belence error(%)	-6

MINOR CONSTITUENTS

Iron .6 pp

OTHER MEASUREMENTS 7.50 Fluoride(F)

Mer	4	Tp	45	Rge	22	Sec	14	Led	11			
Lab no. Index no. Well depth(f) Water level() Top open into Bottom open Altitude(ft) Bedrock eleve TDS(mg/l) Field Cond(m) Field pH	ft) erval(interv	(ft) (a) (f	t) 24g	522 5.0 5.0 5.0		Date Date Samp Samp Owner Hardr Alkal	analy led by le Sou s nam less(a inity !micro	tted /sed(m /rce e cac (as C		Ø1 5 R v(M 11 12 1 30 M 228 638 19	78 79 LL 172 IIN .7

MAJOR CONSTITUENTS

91	mg/1	× •	f total anion
Calcium(Ca)		meq/1	or cation
	60.0	2,99	12.3
Magnesium (Mg)	19.2	1.58	
Spdium (Na)			6.5
	454.0	19.75	80,9
Potassium(K)	2.9	0.07	
Carbonate(CO3)	0.0		0.3
		0,00	0.0
Bigarbonete(HCO3)	798.0	13,08	56.4
Sulphate(504)	469.0		
Chloride (C1)	•	9.76	42,1
	12.0	0.34	1,5
Nitrate(NO3)	0.0	0.00	
Hydrox de (OH)	- # -	0,00	0.0
	₽		
8111ca(8102)	8.5	Total anions(epm)	27 187
Calcium(Acid)	57.0		23,183
Magnesium (Agid)	-	Total cations(epm)	24.396
magnasinu(v610)	12.0	Ion balance error(%)	3.
Calculated TDS	1418.0	TOP halance accorded	· ·
, , , ,		TDS balance error(%)	-4.

MINOR CONSTITUENTS

Iron

4.6 000

OTHER MEASUREMENTS 6.78 Fluoride(F)

Field Temp(C)

0.50 ppm

Index no: 404522 Well depth(ft) Water level(ft) Top open interval(ft) Bottom open interval(ft) 240.0 Altitude(ft) Bedrock elevation(ft) Date submitted Ol 12 78 Date analysed(major) Sampled by R VOGWILL Sample Source BOHAT2 Owners name END Hardness(as CaCO3) 161.3	Mer 4 Tp	45 Rge 22	Sec 14 Lsd 11		
Field Cond(micromhos/cm) Cond(micromhos/cme25C) 1640	Lab no. Index no. Well depth(ft) Water level(ft) Top open interval(ft) Bottom open interval(Altitude(ft) Bedrock elevation(ft) TDS(mg/1) Field Cond(micromhos/s	781057 404522 240.0 29.3 90.0 ft) 240.0	Date sampled Date submitted Date analysed(major) Date analysed(minor) Sampled by R Sample Source Owners name Hardness(as CaCO3) Alkalinity(as CaCO3) Cond(migromhos/cme25C)	27 11 78 91 12 78 5 1 79 VOGWILL BOHAT2 END 161.3 558.4	

MAJOR CONSTITUENTS

		84	
	mg/1	7.0	f total anion
Calcium(Ca)		meq/1	or cation
Manage 1 CM	30.0	1.50	7.5
Magnes um (Mg)	21.0	1.73	
Sodium(Na)	-		8,6
	384,0	16,70	63.5
Potassium(K)	∘2.5	0.06	0.3
Cerbonate (CO3)	0.0	•	
Bicarbonate(HCO3)		0.00	0.0
	698.0	11,44	58,2
Sulphate(804)	379.0	7.89	
Chloride(Cl)	12.0		40.1
	_	0.34	1.7
Nitrate(ND3)	0.0	0.00	0.0
Hydrox de (OH)		~ ~ ~	0,0
Silica(8102)	0.6	.	
	9.6	Total anions(epm)	19.670
Calcium (Acid)	57.0	Total cations(epm)	19,992
Magnestum (Agid)	14.0		- .
Calculated TDS		Ion belance error(%)	1.
earratated 102	1181.3	TDS balance error(%)	485.

MINOR CONSTITUENTS

OTHER MEASUREMENTS 7.40 Fluoride(F)

44 ---

Men 4	Tp	45	Rge	22	Sec 14 Lad 11			
Leb no. Index no. Hell depth(ft) Water level(ft) Top open interval Bottom open inter Altitude(ft) Bedrogk elevation TDS(mg/!) Field Cond(micromi	vel († (ft)	40 2 (t) 2	1962 4522 40.0 30.0 90.9 40.0		Date analysed(major) Date analysed(minor) Sampled by Sample Source	4 1 8 1 5 VOG 80 1 1 5 6	2 1 WIL	78 78 79 L 13 14 13

MAJOR CONSTITUENTS

Calcium(Ca) Magnesium(Mg) Sodium(Na) Potessium(K) Carbonate(CO3) Bicarbonate(HCO3) Suiphate(SO4) Chioride(C1) Nitrate(NO3) Hydroxide(OH)	mg/! 29.0 16.3 454.0 2.5 12.0 683.0 463.0	meq/1 1.45 1.34 19.75 0.06 0.40 11.19 9.64 0.34 0.00	f total anion or cation 6.4 5.9 87.4 0.3 1.9 51.9 44.7 1.6 0.0
Silice(SiD2) Celcium(Acid) Magnesium(Acid) Celculated TDS	8.8 53.0 14.0 1333,4	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	21.573 22.600 2. -3.

MINOR CONSTITUENTS

Iron

2.4 000

OTHER MEASUREMENTS
6.30 Fluoride(F

Field Temp(C)

0.50 ppm

Men 4	Tp e 4	5 Rge	22	Sec	14	Lad	11			
								D	M	¥
Leb no.		781063		Dete	sempi	e d		4	12	
Index no.		404522			submi				12	
Well depth(ft)		240.0					najor)	5	-	79
Water level(ft		30.0					ninor)	•	•	, ,
Top open inter		90.0			ed by		71101-7	V	GW	7 I I
Bottom open in	terval(ft				e \$0u				30H	_
Altitude(ft)								-		
	E				# nam					ND
Bedrock elevat	10n(Tt)			Hardr	055(a	s CaC	(20:		233	5.8
TD\$(mg/1)		1270.0					(aCO3)		628	
Field Cond(mig	romhos/cm)					(cm+25C)			60
Field pH	- 1850." -	-		Lab p						8

MAJOR CONSTITUENTS

		, x ¢	f total anion
	mg/1	meq/1	or cation
Calclum(Ca)	64.0	3,19	14.9
Magnestum (Mg)	18.0	1.48	6.9
Sodium (Na)	384.0	16.70	77.7
Potassium(K)	4.2	0.11	0.5
Carbonate(CO3)	0.0	0.00	0.0
Bicarbonate(HCQ3)	786.0	12.88	61.5
8ulphate(804)	360.0	7.50	35,8
Chioride (Ci)	20.0	0.56	2,7
Nitrate(NO3)	0.4	0.01	0.0
Hydroxide(OH)	•		
Silica(8102)	9.7	Total enions(epm)	20.949
Colcium(Acid)	61.0	Total cations(epm)	21.485
Magnesium(Acid)	17.0	Ion balance error(%)	
Calculated TDS	1246.8	TDS belence error(%)	-2,

MINOR CONSTITUENTS

Iron

Field Temp(C)

OTHER MEASUREMENTS 6.25 Fluoride(F)

Men	4 Tp	45 Rge	22	Sec 14	Lad 11			
						D	M	Y
Lab no.		781072		Date sampl	ed	11	12	
Index no.		404522		Date submi	tted		12	
Well depth(ft)	240.0			(nolor)	9		79
Water level(f	t)	30.0			sed(minor)		•	, ,
Top open inte	rval(ft)	90.0		Sampled by		V)GW]	71.1
Bottom open i				Sample Sou			SOHA	
Altitude(ft)				Owners nam			30M	
Bedrock eleva	tion(ft)			Hardness (a		•	,	
TDS(mg/1)	, , , , , , , , ,	1378.0			(as CaCO3)		229	-
Field Cond(mi	anambaa/a	.)					636	-
Field pH	A LOWINGS & CL	H .			mhos/cm#25C)		30
. 1610 bu				Lab pH			7	.,

MAJOR CONSTITUENTS

		· * * * * * * * * * * * * * * * * * * *	f total ion
• • • • •	mg/1	meq/i	or cation
Calcium(Ca)	64.0	3,19	13,2
Magnesłum(Mg)	17.0	1.40	5,8
Sodium(Na)	449.0	19,53	80.7
Potassium(K)	2.5	0.06	0.3
Carbonate(CO3)	0.0	0.00	0.0
Bicarbonate(HCO3)	795.0	13.03	56.4
Sulphate(804)	464.0	9.66	41.8
Chloride(Cl)	14.0	0.39	1,7
Nitrate(NO3)	9.2	0.00	0.0
Hydroxide(OH)	- 4	· •	
Siliqa(8102)	10.0	Total anions(epm)	23.089
Calgium(Acid)	60.0	Total cations(epm)	24.187
Magnesium (Agid)	16,0	Ion belence error(%)	
Calculated TDS	1411,6	TDS balance error(%)	

MINOR CONSTITUENTS

Iron

4 00

OTHER MEASUREMENTS 6.38 Fluoride(F)

Field Temp(C)

3.40 ppm

Men	4 Tp	45 Rge	22	Sec 14 Lad 11	
Lab no. Index no. Well depth(it Water level(it) Top open inte Bottom open inte Altitude(it) Bedrock eleva TDS(mg/l) Field Cond(min	t) rval(ft) nterval(1 tion(ft)	1212.0		Date submitted Date analysed(major) Date analysed(minor)	D M Y 1 12 78 3 12 78 9 1 79 VOGWILL BOHAT4 END 247.0 634.4 1780 7.7

MAJOR CONSTITUENTS

Calcium(Ca) Magnestum(Mg) Sodium(Na) Potassium(K)	mg/1 66.0 20.0 390.0 2.1	# o meq/ 3,29 1,65 16,96 0,05	f total anion or cation 15.0 7.5 77.3 0.2
Carbonate(CO3) Bicarbonate(HCO3) Sulphate(804) Chloride(Cl) Nitrate(NO3) Hydroxide(OH)	0.0 793.0 331.0 16.0 0.2	0.00 13.00 6.89 0.45 0.00	0.0 63.9 33.9 2.2 0.0
Silice(SiO2) Calcium(Acid) Magnesium(Acid) Calculated TDS	10.0 62.0 18.0 1225.2	Total anions(epm) Total cations(epm) Ion balance error(%) TDS balance error(%)	20.344 21.957 4.

MINOR CONSTITUENTS

Iron

8.6 ppm

OTHER MEASUREMENTS 7.18 Fluoride(F)

Field Temp(C)

	Men	4	Tp	45	Rge	22	Sec	14	Led	11			
Lab no. Index no. Well dept Water lev Top open Bottom op Altitude(Bedrock e TDS(mg/l) Field Con- Field pH	h(fi el(fi en i ft)	it) rval inter	(ft)	48 2 t) 2	1089 4522 40.0 29.3 92.0 40.0	•	Date Date Date Sampl Sampl Owner Hardn Alkal	enaly ed by e Sou s name ess(a) inity mignor	tted sed(n sed(n rce cococococococococococococococococococ	major) minor)	0.4 1.0 R_V(12 Ø1 1 30HA 10 M 250 634	79 79 LL 175 11N

MAJOR CONSTITUENTS

	4.6	X o	f total anion
Ø - 1	mg/1	meq/1	or cation
Calcium(Ca)	64.0	3.19	
Magnes (um (Mg)	22.0		13.1
Sodium (Na)	•	1.81	7.4
	443.0	19.27	79.2
Potassium(K)	2.1		
Carbonate(CO3)		0,05	0.2
	0.0	0.00	0.0
Bicarbonate (HCO3)	793.0	13.00	
Sulphate(SO4)	484.0	-	55,4
Chloride(C1)	•	10,08	42.9
AUTOLICATORS	14,0	0.39	1.7
Nitrate(NO3)	0.0	0.00	
Hydroxide(OH)	- • •	0100	0.0
Silica(SiO2)			
	8.9	Total anions(epm)	23.470
Calgium (Agid)	62.0	Total cations(epm)	-
Magnesium (Acid)	21.0	To be to the temperature of the	24,327
Calculated TDS		Ion balance error(%)	2.
AGIÉGIAFAD IDŽ	1427.9	TDS belance error(X)	14.

MINOR CONSTITUENTS

Iron

2.0 000

OTHER MEASUREMENTS 5.80 Fluoride(F)

Field Temp(C)

8.58 ppm

M	Pr	4	Tp	45	Rge	22	3ec	14	Led 1	1				
Lab no. Index no. Well depth Hater leve! Top open in Bottom open Altitude(fit Bedrogk els TDS(mg/l) Field Cond(Field pH	1 (1	it) rva nte	rval († n(ft)	404 24 2 2 t) 24	090 1522 10.0 20.3 20.0		Date Date Samp Samp Owner Hardr	anai anai ied b ie \$0 rs na resa(iinit (migr	itted yeed(me yeed(mi) y urce	Jor) nor) R 3)	04 10 V	0GW BOH 262 620	78 79 79 ILL AT5 END 2.6	章

MAJOR CONSTITUENTS

		x (of total anion
Caladanda	mg/1	meq/1	or cation
Calcium(Ca)	64.9	3,19	(5)
Magnes (um (Mg)	25.0		14,5
Sodium (Na)		2.06	9.4
	384.0	16,70	76.0
Potessium(K)	1.3	0.03	
Carbonate(CO3)	0.0	0.00	0.2
Bicarbonate (HCO3)	783.0		0.0
Sulphate (804)		12,83	64,2
	339.0	7.06	35,3
Chloride (C1)	4.0	0.11	
Nitrate(NO3)	0.0		0,6
Hydrox de (OH)	0,0	0.00	0.0
Silica(S102)	_ =		
	8.9	Total anions(epm)	20.005
Calcium (Acid)	57.0	Total gations(epm)	
Magnesium (Acid)	25.0	Too belonce and the	21,987
Calculated TDS	-	Ion balance error(x)	5.
	1211.2	TDS balance error(%)	#4 ,

MINOR CONSTITUENTS

Iron

1 ppm

OTHER MEASUREMENTS 6.18 Fluoride(F)

Field Temp(C)